

Polarimetric study of the liquid crystal panels. Optimization for diffractive optics

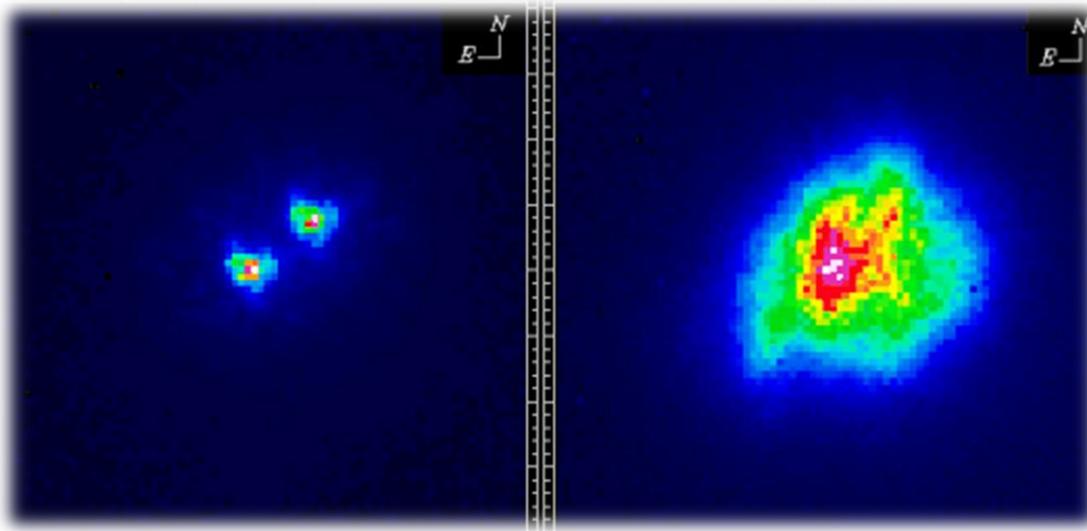
María J. Yzuel

Professor Emeritus
Department of Physics
Universitat Autònoma de Barcelona (Spain)

Vice President ICO Bureau (International Commission for Optics)
SPIE 2009 President



LCDs applications

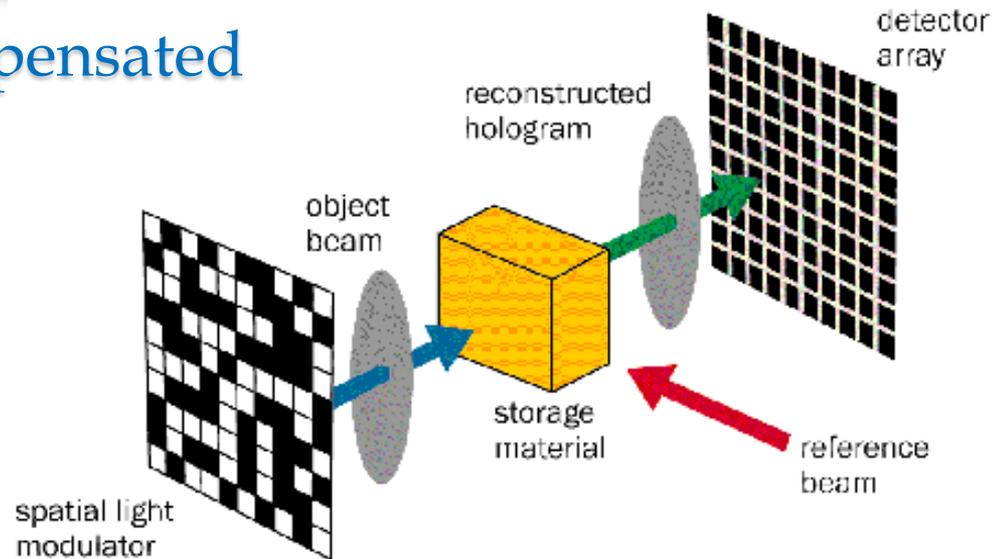


Compensated

Uncompensated

- Adaptive Optics: Binary Stars

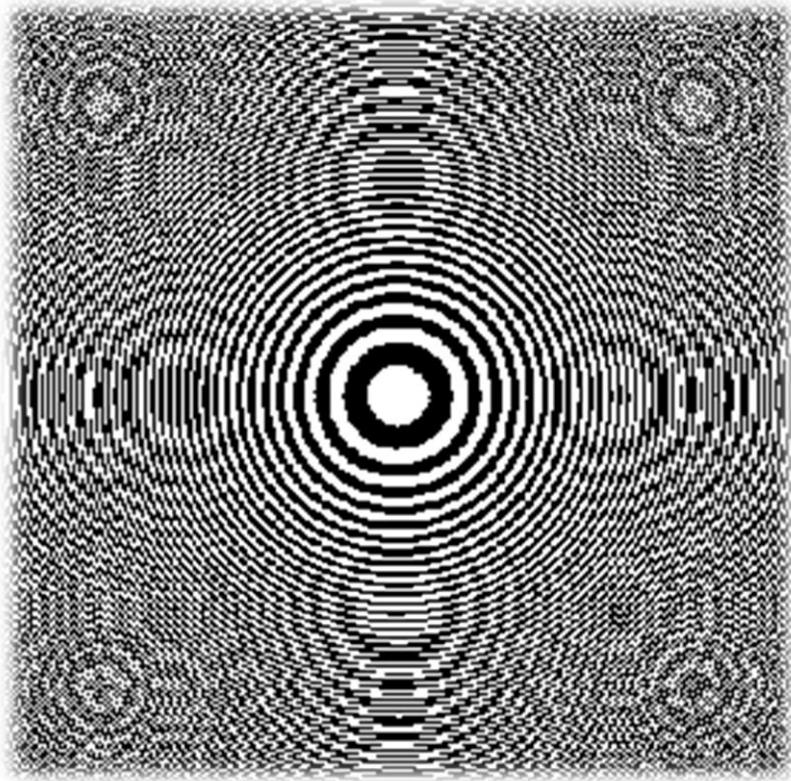
- Holographic data storage



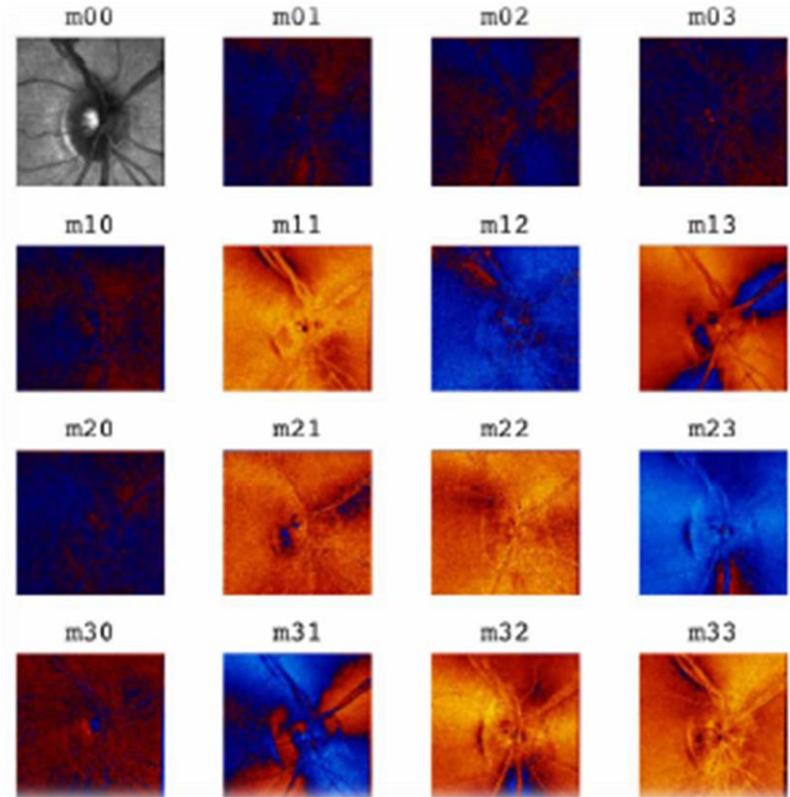
Basic holographic data storage set-up

LCDs applications

- **Diffraction Optics**



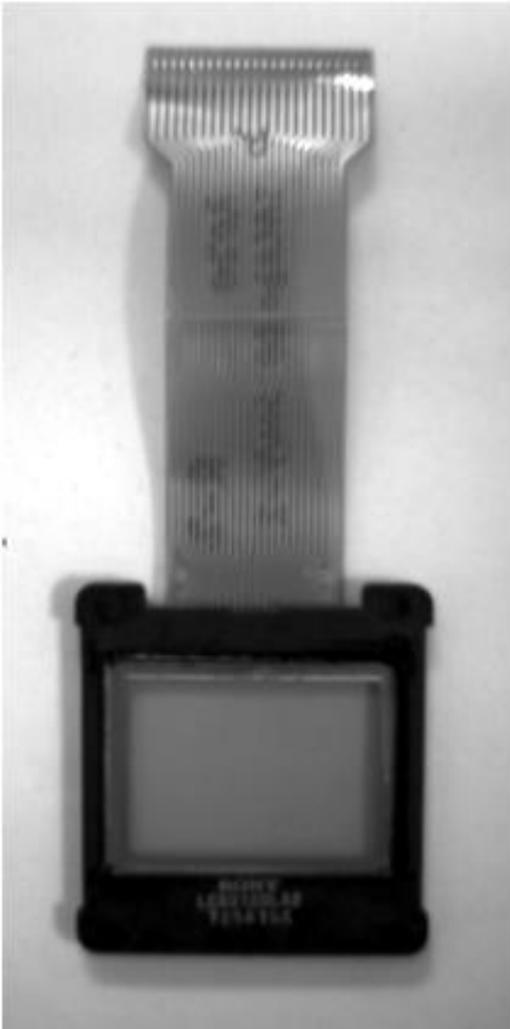
- **Medical Optics:
Polarimeters**



Mueller matrix images of the optic nerve head.

LCD from Video projectors

Transmission Twisted Nematic Liquid Crystal devices



TN-LCSLM: Sony Model LCX012BL;
VGA (640 x 480)
Videoprojector Sony VPL-V500

LCoS display

Reflective Liquid Crystal on Silicon devices

Twisted Nematic
kit LC-R2500 by Holoeye



Parallel Aligned
kit Pluto by Holoeye



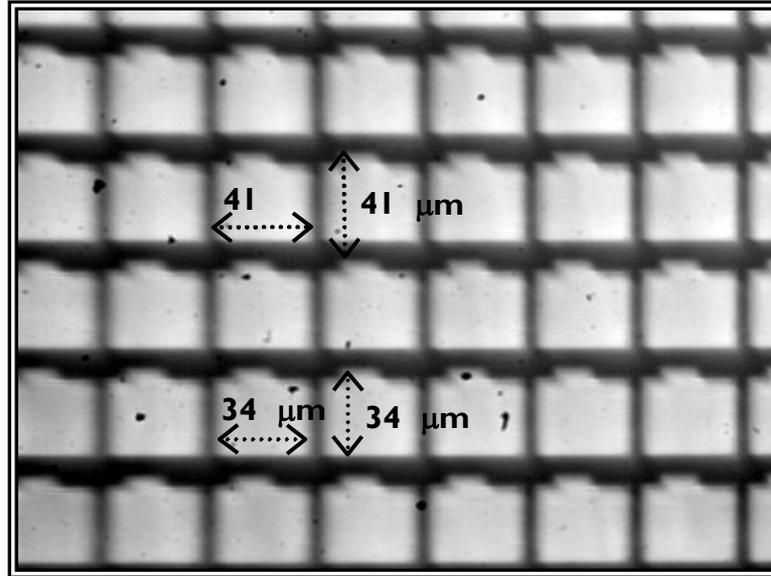
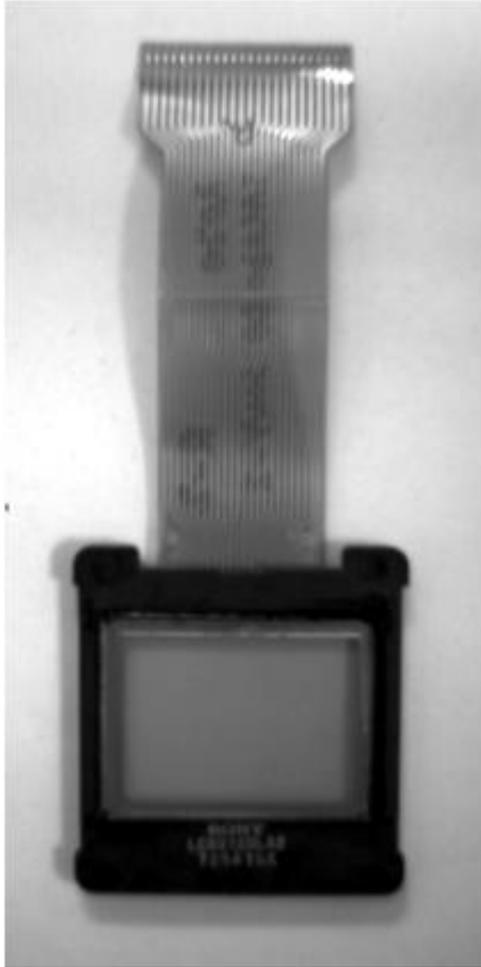
CONTENTS

- **Polarimetric study of the liquid crystal panels**
 - Non Depolarizing devices
 - Depolarizing devices
 - Modulation Optimization
- **Use of commercial LCDs in diffractive Optics**
 - Color Pattern Recognition
 - Apodization
 - Lens multiplexing

- Polarimetric study of the liquid crystal panels

Non Depolarizing devices

Polarimetric study of the liquid crystal panels

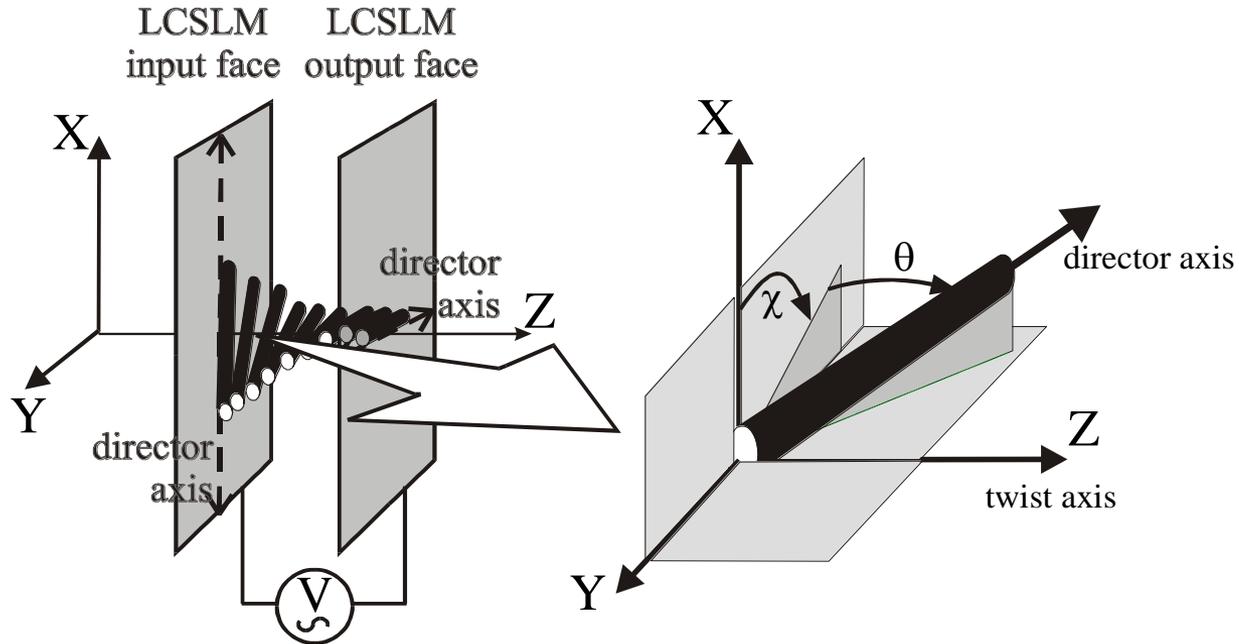


Transmission Twisted Nematic Liquid Crystal devices

TN-LCSLM: Sony Model LCX012BL;
VGA (640 x 480)

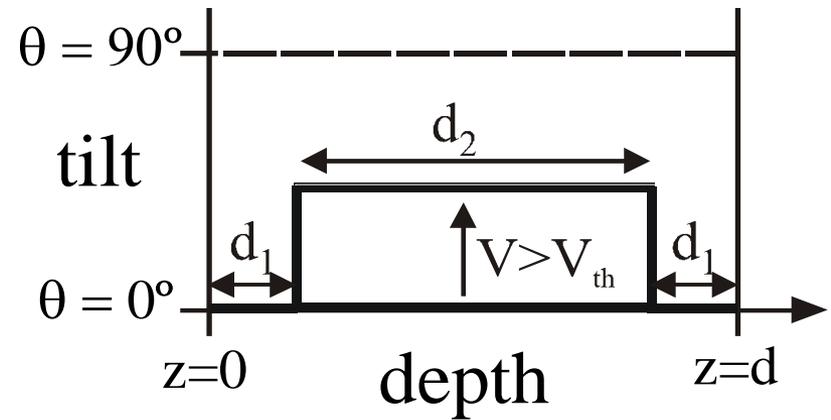
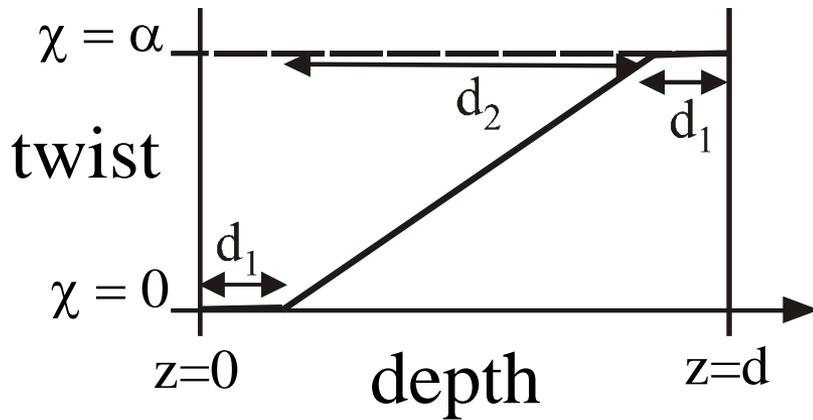
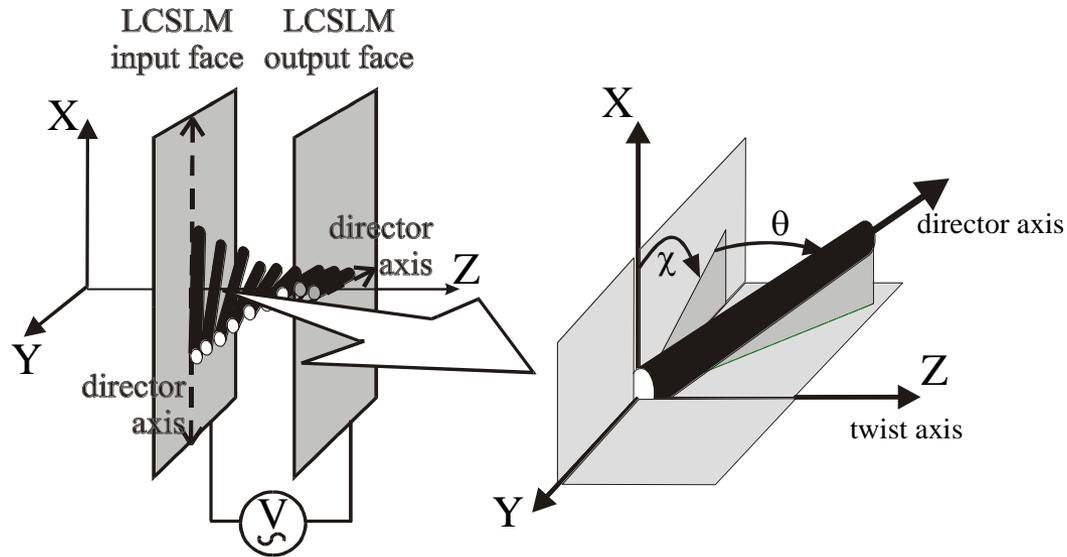
Videoprojector Sony VPL-V500

Simplified model



$$\frac{1}{n_e^2(\theta)} = \frac{\cos^2(\theta)}{n_{\parallel}^2} + \frac{\sin^2(\theta)}{n_{\perp}^2}$$

Simplified model



Jones Matrix

$$M'_{LCSLM}(\alpha, \beta, \delta) = \exp(-i(\beta + 2\delta))R(-\alpha) \begin{pmatrix} X' - iY' & Z \\ -Z & X' + iY' \end{pmatrix}$$

$$X' = X \cos 2\delta - Y \sin 2\delta$$

$$X = \cos \gamma$$

$$Y' = X \sin 2\delta + Y \cos 2\delta$$

$$Y = \frac{\beta}{\gamma} \sin \gamma$$

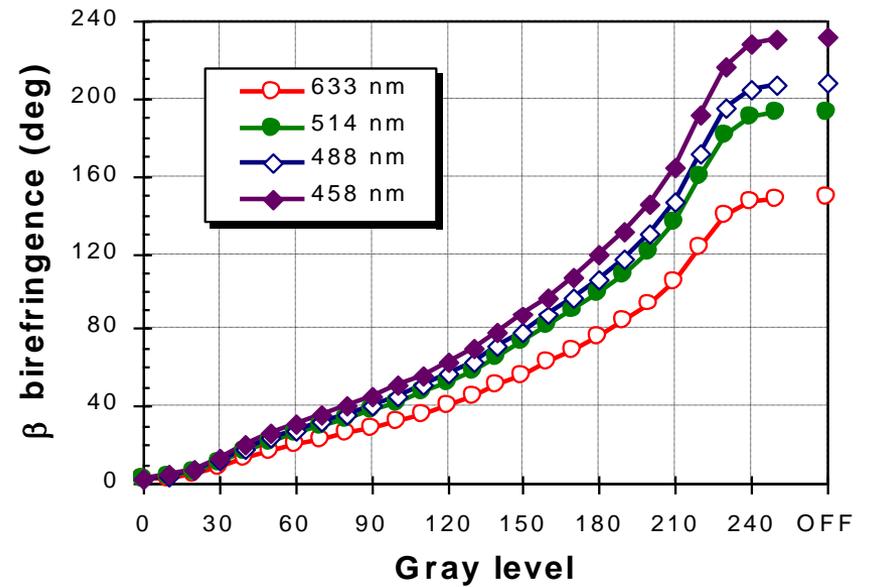
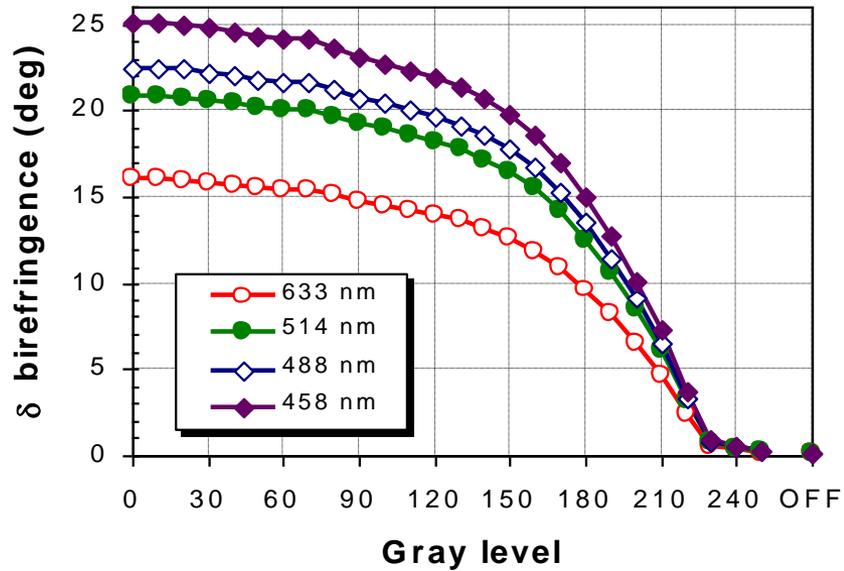
$$Z = \frac{\alpha}{\gamma} \sin \gamma$$

$$\gamma = \sqrt{\alpha^2 + \beta^2}$$

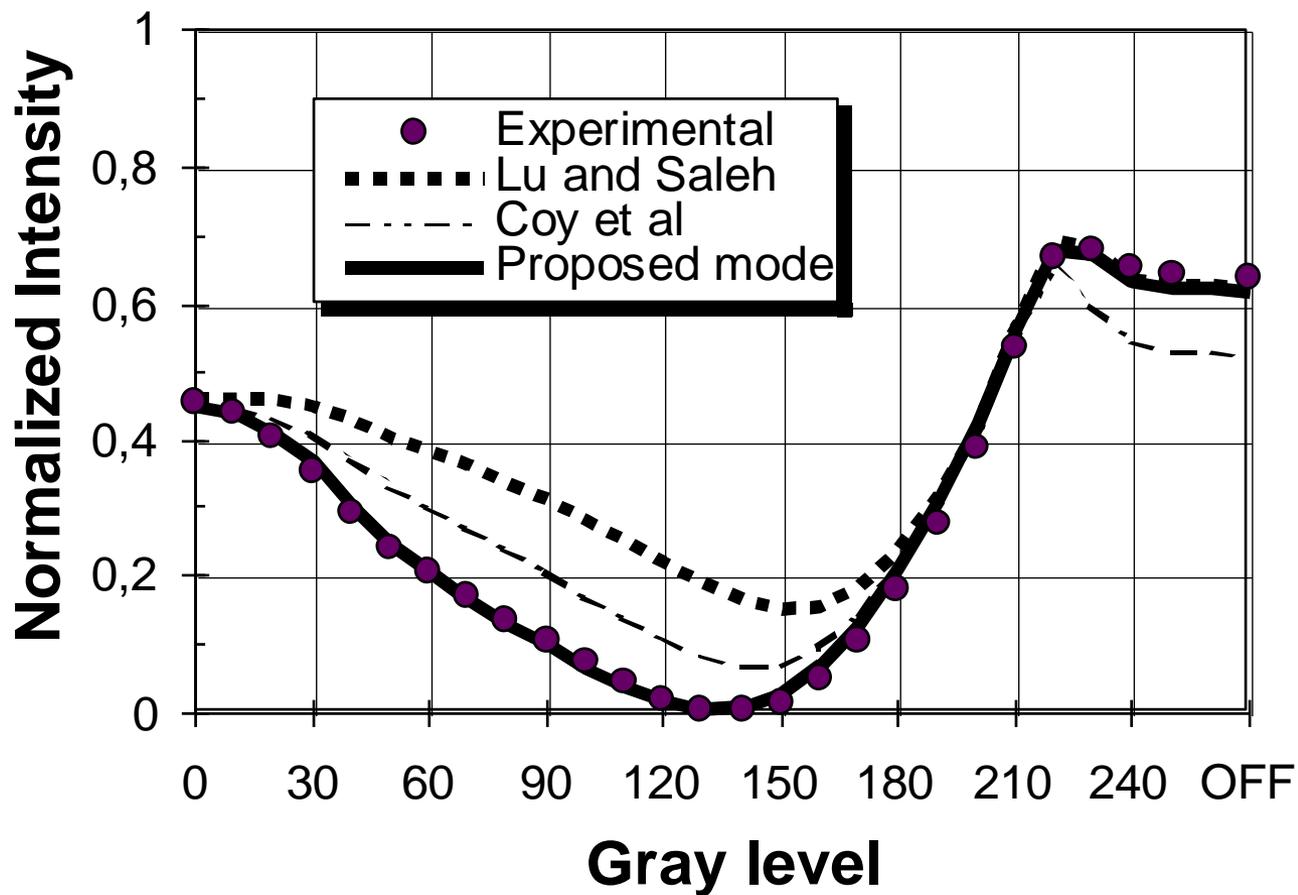
$$\delta(V) = \pi d_1(V) \Delta n_{max} / \lambda$$

$$\beta(V) = \pi d_2(V) \Delta n(V) / \lambda$$

Measured Parameters



Predictive capability of the model

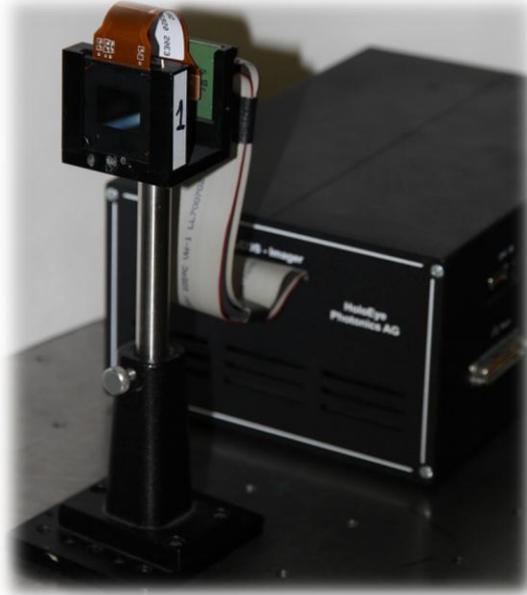


- Polarimetric study of the liquid crystal panels

Depolarizing devices

Technical features of the used TNLCoS

Twisted Nematic LCoS display



Twist of the LC molecules director along the cell



- Philips model X97c3A0.
- Kit LC-R2500 by Holoeye
- 2.46 cm diagonal reflective LCoS display of the 45° twisted nematic type.
- XGA resolution (1024x768)
- Digitally controlled gray scales with 256 gray levels.
- Square pixels with a center to center separation of 19mm.
- 93% fill factor.

Technical features of the used PALCoS

Parallel Aligned LCoS display



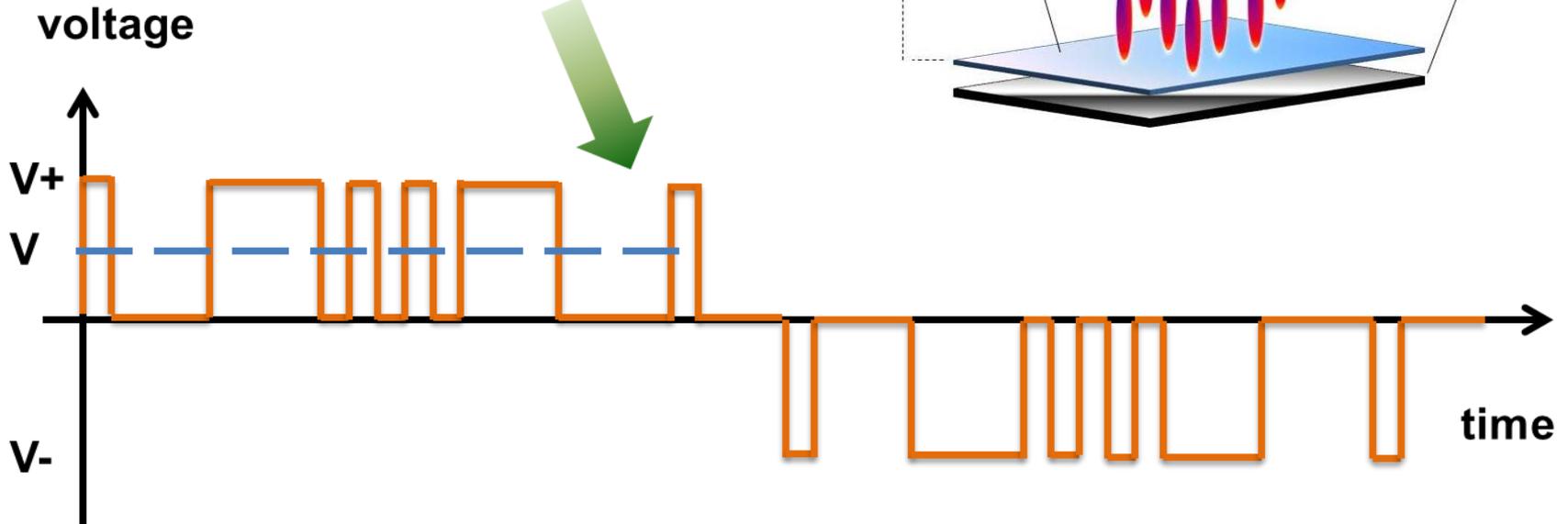
*LC
molecules
parallel
aligned*



- PLUTO Spatial Light Modulator (SLM) distributed by Holoeye.
- Diagonal display of 1.8 cm.
- High resolution: 1920 x 1080.
- Small pixel size : 8 μ m.
- Fill factor of 87%.
- Different gamma corrections and electrical sequences available.

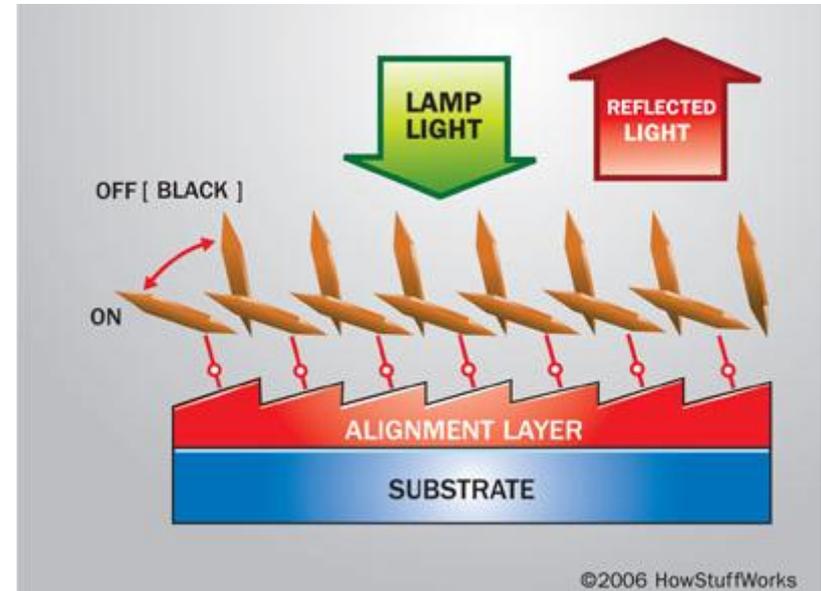
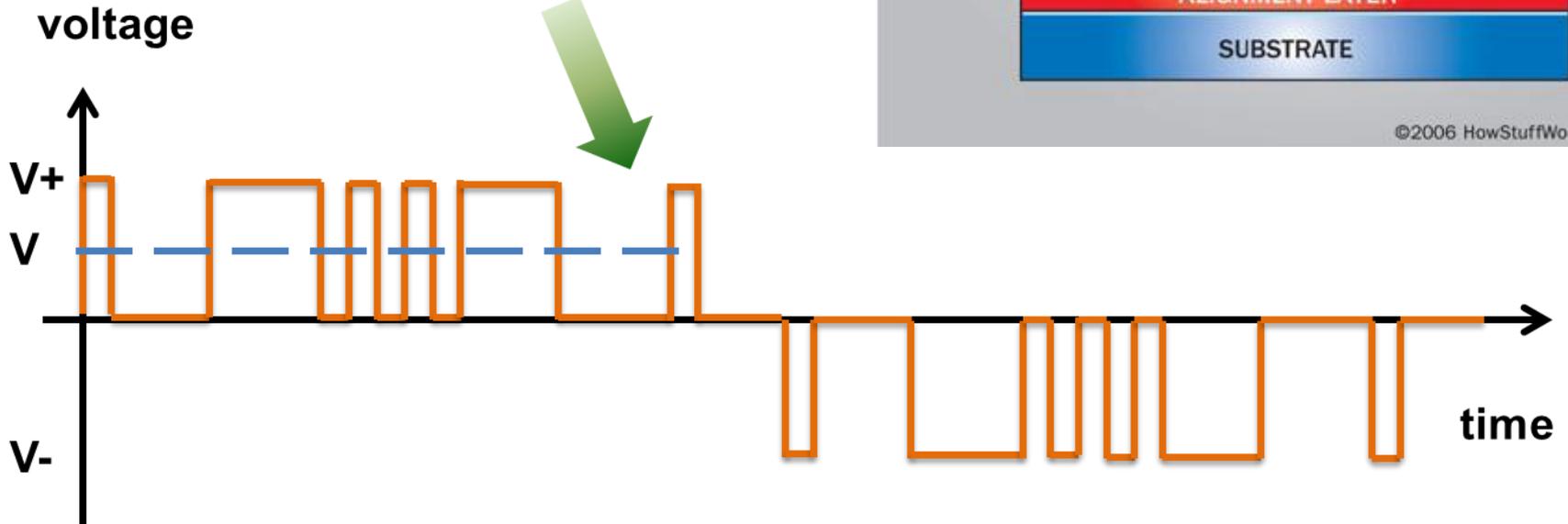
Time-fluctuations in LCoS displays

Digital addressing schemes:
Pulse Width Modulation



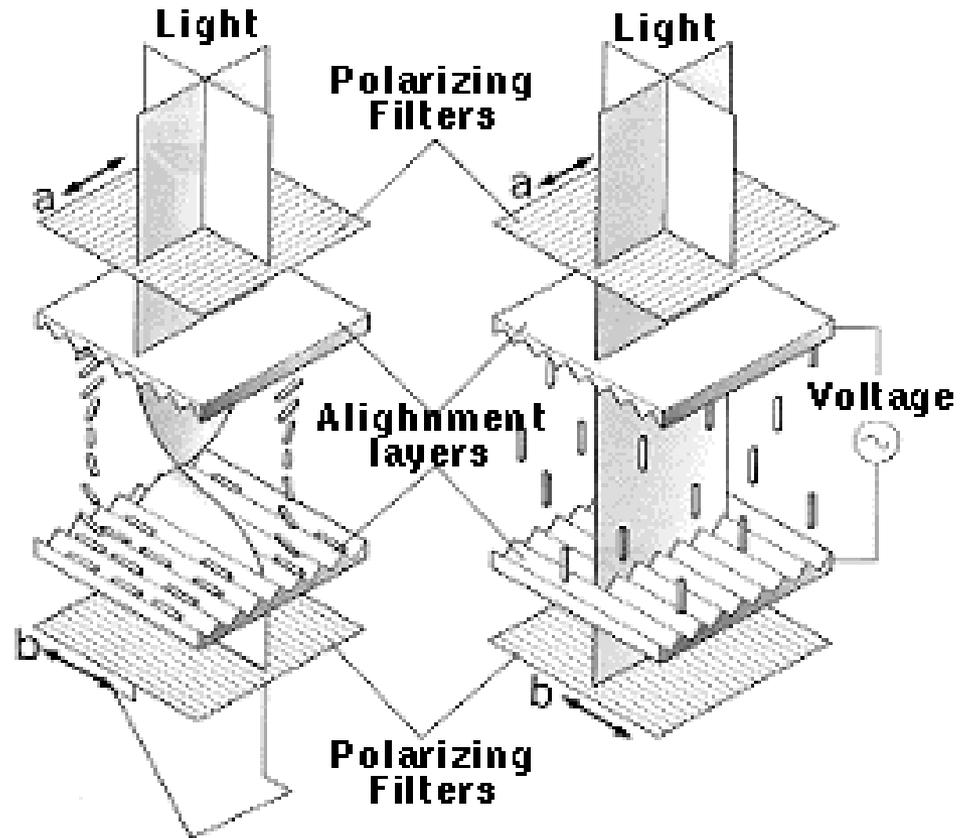
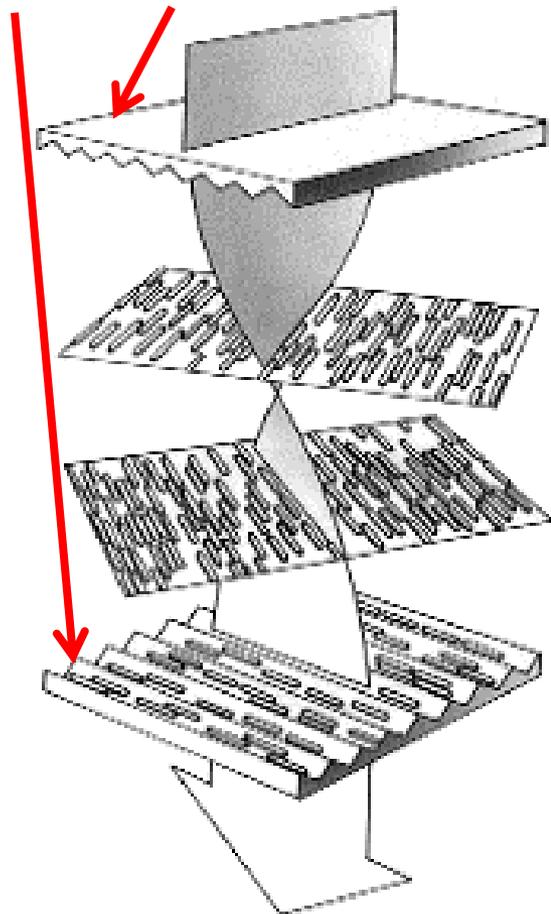
Time-fluctuations in LCoS displays

Digital addressing schemes :
Pulse Width Modulation



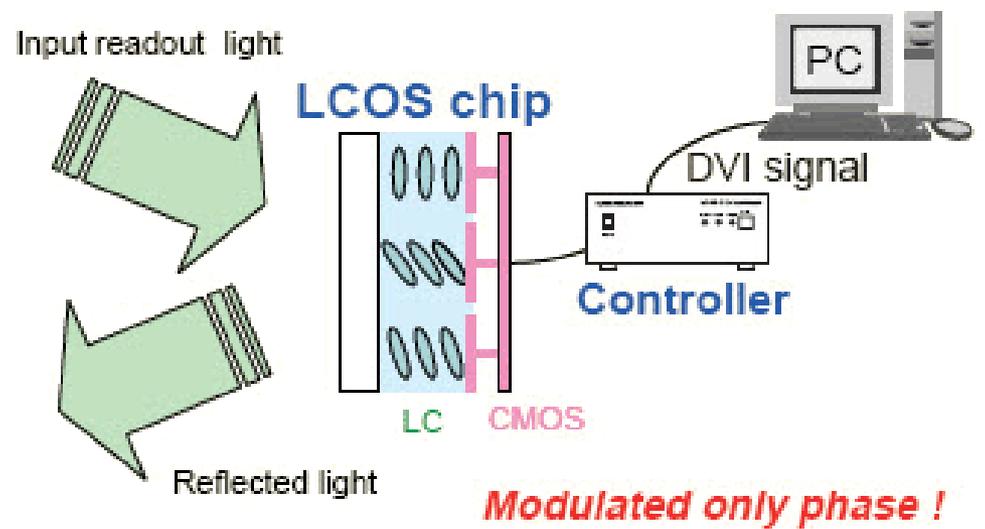
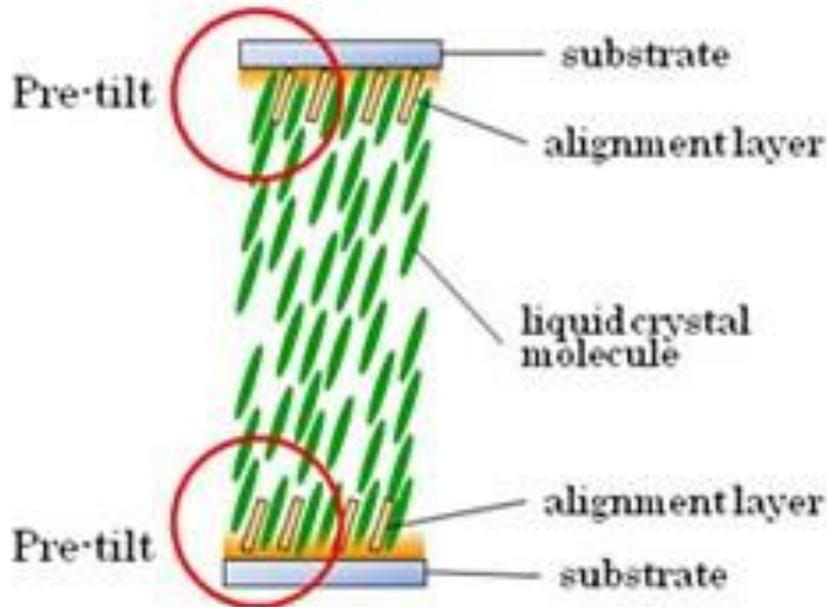
Twisted Nematic

Alignment layers



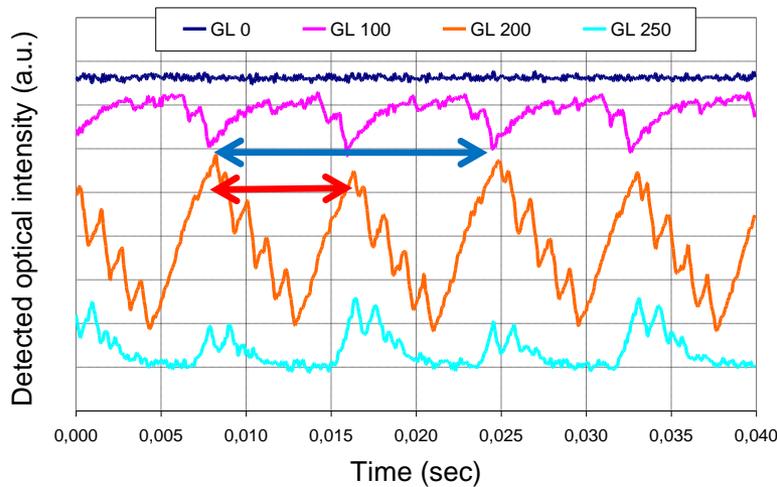
Parallel Aligned

Sony's independently developed "FPA"
liquid crystal alignment technique

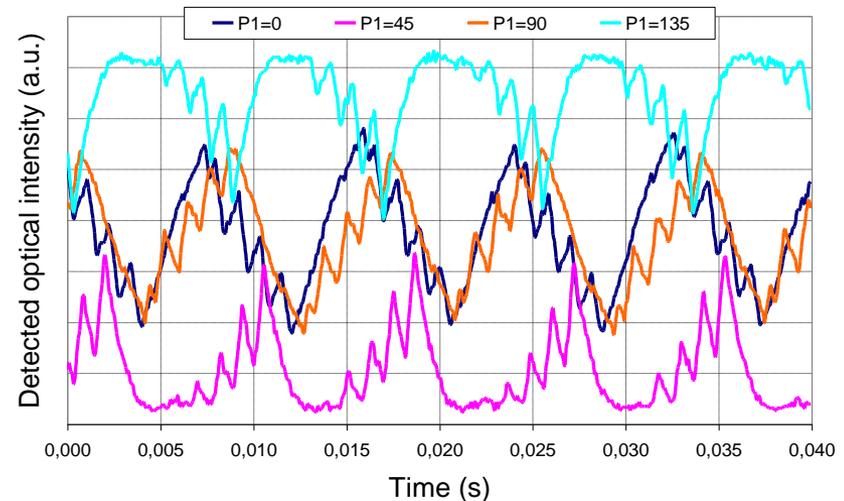


Time-fluctuations in LCoS displays

- Reflected intensity measurements (incident angle equal to 2°) acquired with a Tektronix TDS3012B Digital Oscilloscope



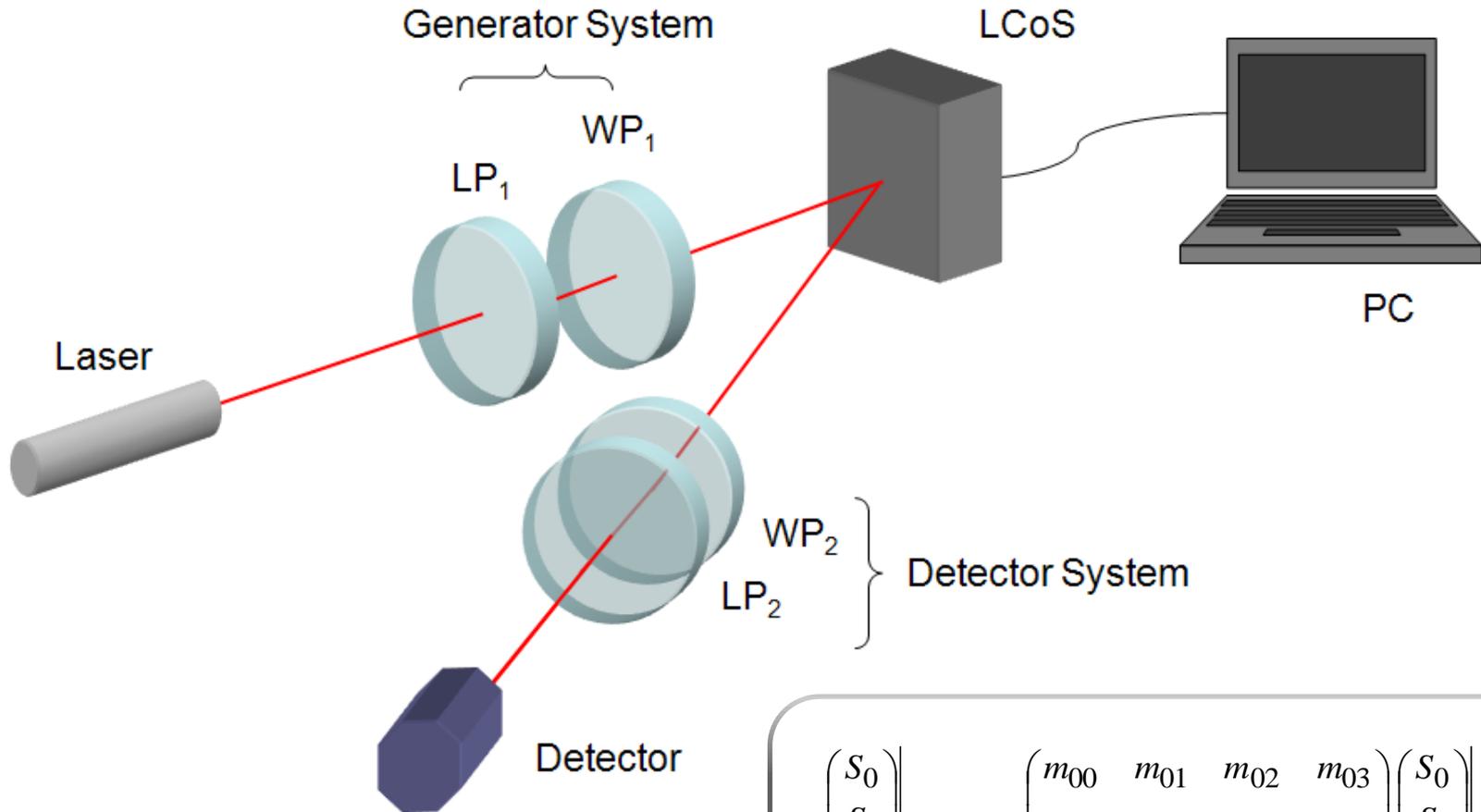
- Fixed polarizers (at 0° with respect to the vertical of the lab)



- Fixing gray level (at 200) and output polarizer (at 0° Vertical-Lab)

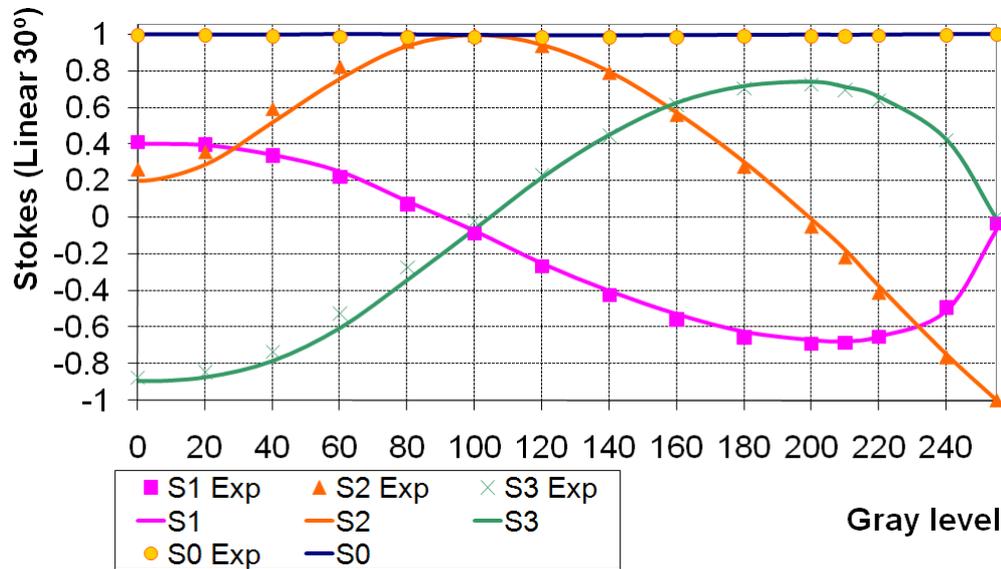
- Intensity oscillates with a period of **~ 17 ms** (~ 60 Hz), with a sub period of **~ 8 ms** (~ 120 Hz)

LCoS display characterization set-up

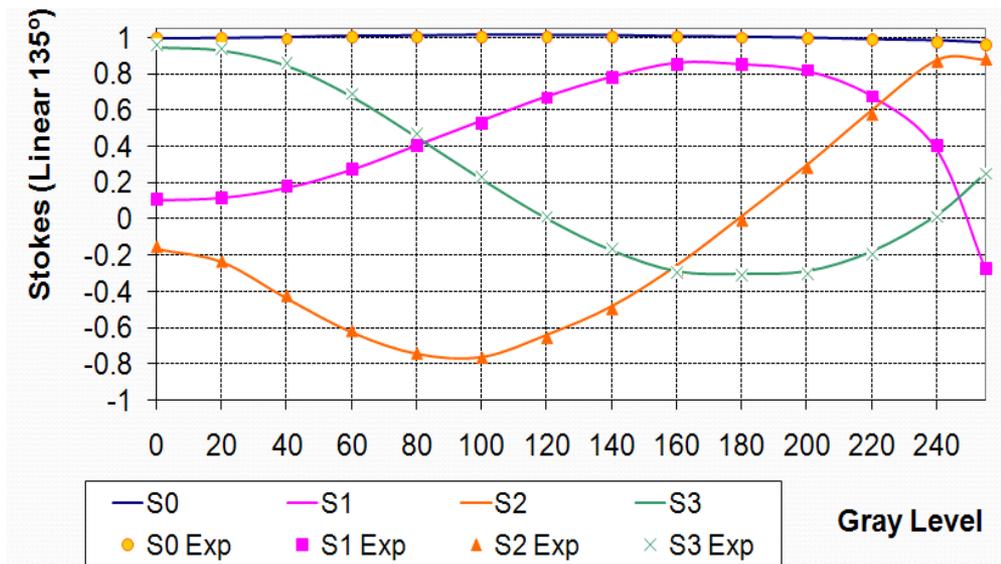


$$\begin{pmatrix} S_0 \\ S_1 \\ S_3 \\ S_4 \end{pmatrix}_{Output} = \begin{pmatrix} m_{00} & m_{01} & m_{02} & m_{03} \\ m_{10} & m_{11} & m_{12} & m_{13} \\ m_{20} & m_{21} & m_{22} & m_{23} \\ m_{30} & m_{31} & m_{32} & m_{33} \end{pmatrix} \begin{pmatrix} S_0 \\ S_1 \\ S_3 \\ S_4 \end{pmatrix}_{Input}$$

LCoS Mueller matrices validation



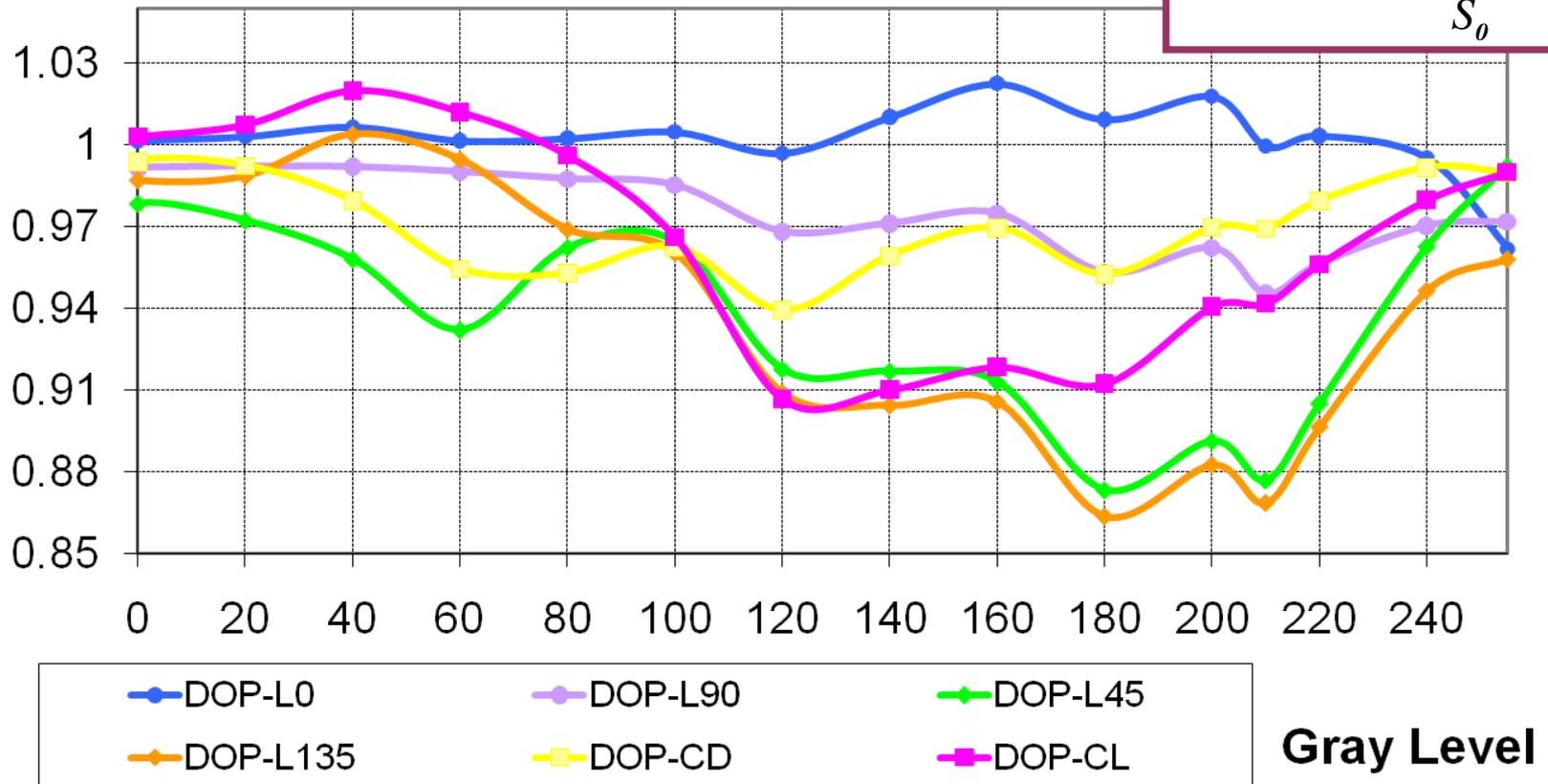
Non Synchronous characterization method.



Synchronous characterization method.

Degree of Polarization (DOP)

$$DOP = \frac{(S_1^2 + S_2^2 + S_3^2)^{1/2}}{S_0}$$



Degree of polarization as a function of the gray level and the incident state of polarization for quasi-normal incidence.

Polar decomposition of the Mueller matrix

$\mathbf{M} = \mathbf{M}_\Delta \mathbf{M}_R \mathbf{M}_D$ Depolarization, retardance, and diattenuation

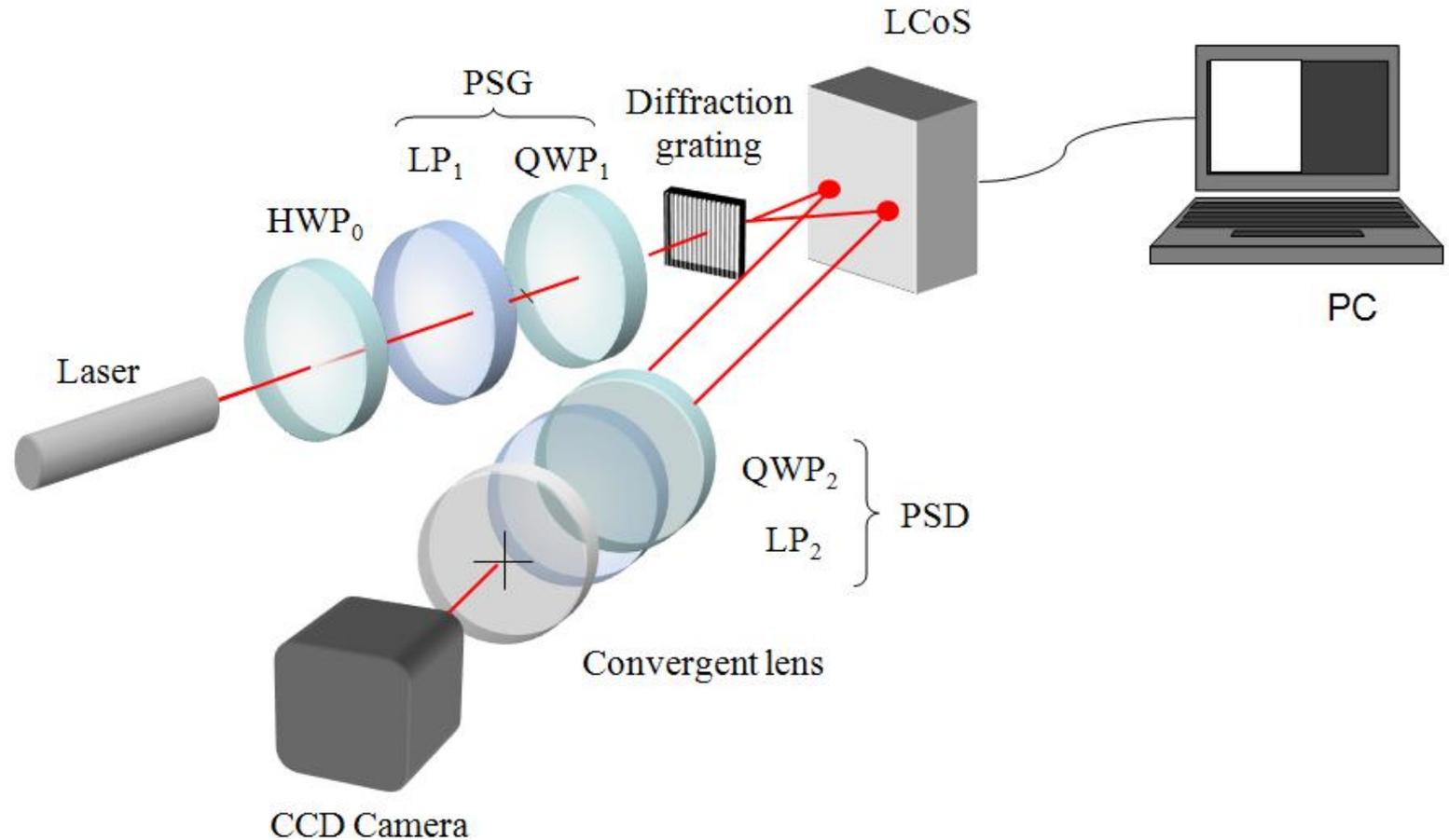
$$\mathbf{M} = \mathbf{M}_\Delta \mathbf{M}_R = \begin{pmatrix} 1 & \vec{0}^T \\ \vec{P}_\Delta & m_\Delta \end{pmatrix} \cdot \begin{pmatrix} 1 & \vec{0}^T \\ \vec{0} & m_R \end{pmatrix} = \begin{pmatrix} 1 & \vec{0}^T \\ \vec{P}_\Delta & m_\Delta m_R \end{pmatrix}$$

The **Jones matrix** of a non-absorbing polarization element

$$\mathbf{J}_R = e^{-i\beta} \begin{pmatrix} A & B \\ -B^* & A^* \end{pmatrix} = e^{-i\beta} \begin{pmatrix} A_{\text{Re}} - iA_{\text{Im}} & B_{\text{Re}} - iB_{\text{Im}} \\ -B_{\text{Re}} - iB_{\text{Im}} & A_{\text{Re}} + iA_{\text{Im}} \end{pmatrix}$$

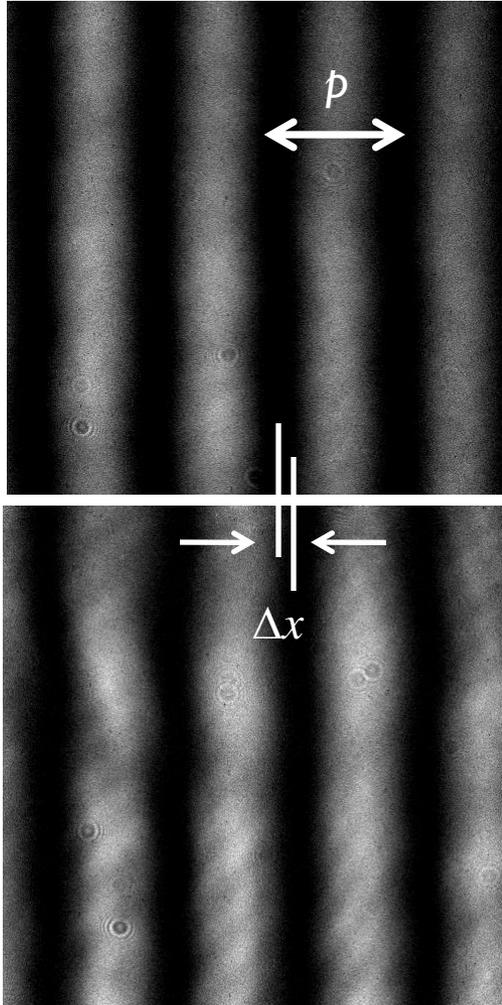
$$A_{\text{Re}}^2 + A_{\text{Im}}^2 + B_{\text{Re}}^2 + B_{\text{Im}}^2 = 1$$

Phase measurement set-up



 Interference method based set-up for experimental phase measurements.

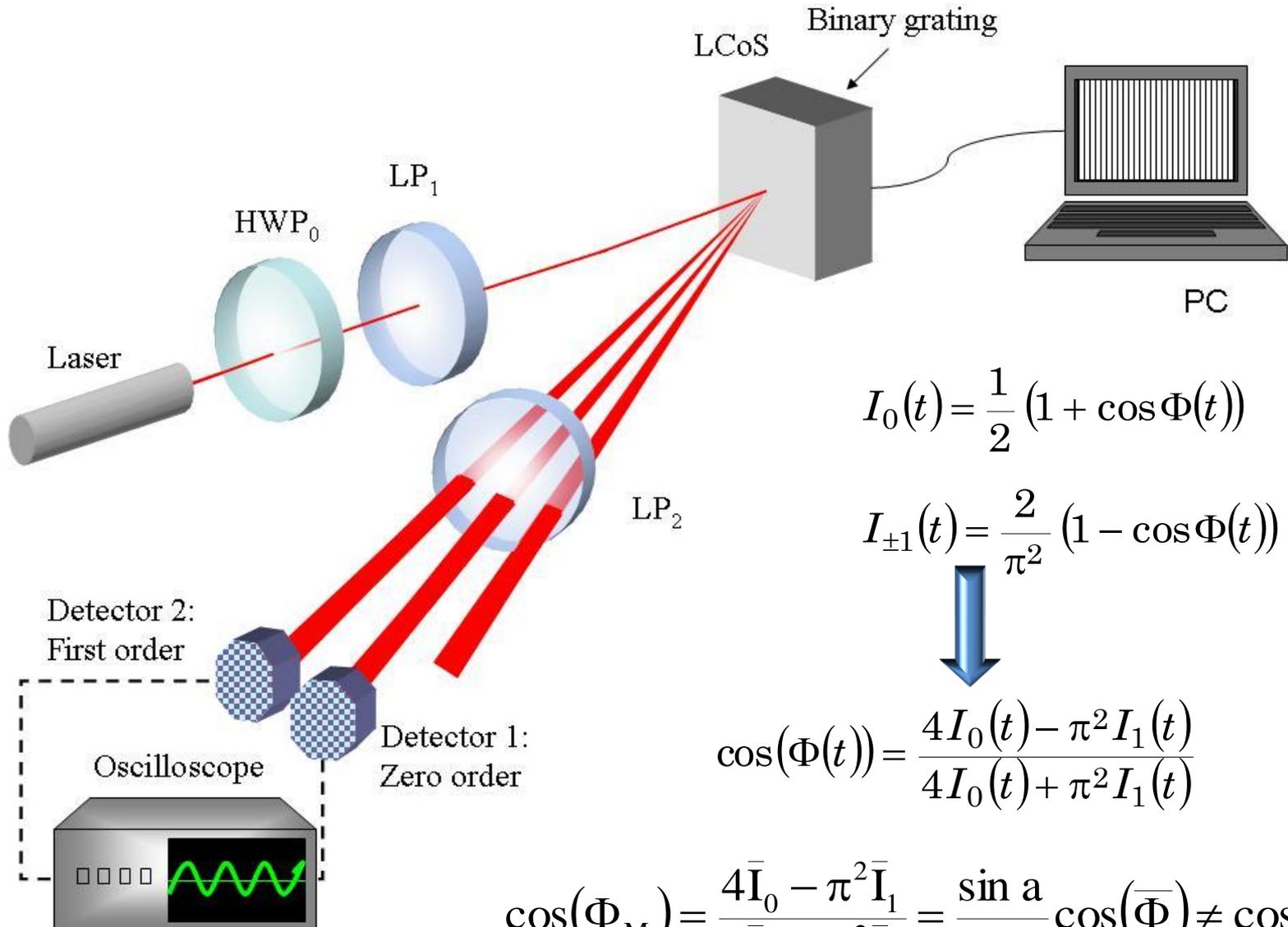
Phase measurement set-up



$$I(x) = 2I_0(1 + \cos(2\pi px + \Phi))$$

 Interference method based set-up for experimental phase measurements.

Time-fluctuations of the phase



$$I_0(t) = \frac{1}{2} (1 + \cos \Phi(t))$$

$$I_{\pm 1}(t) = \frac{2}{\pi^2} (1 - \cos \Phi(t))$$

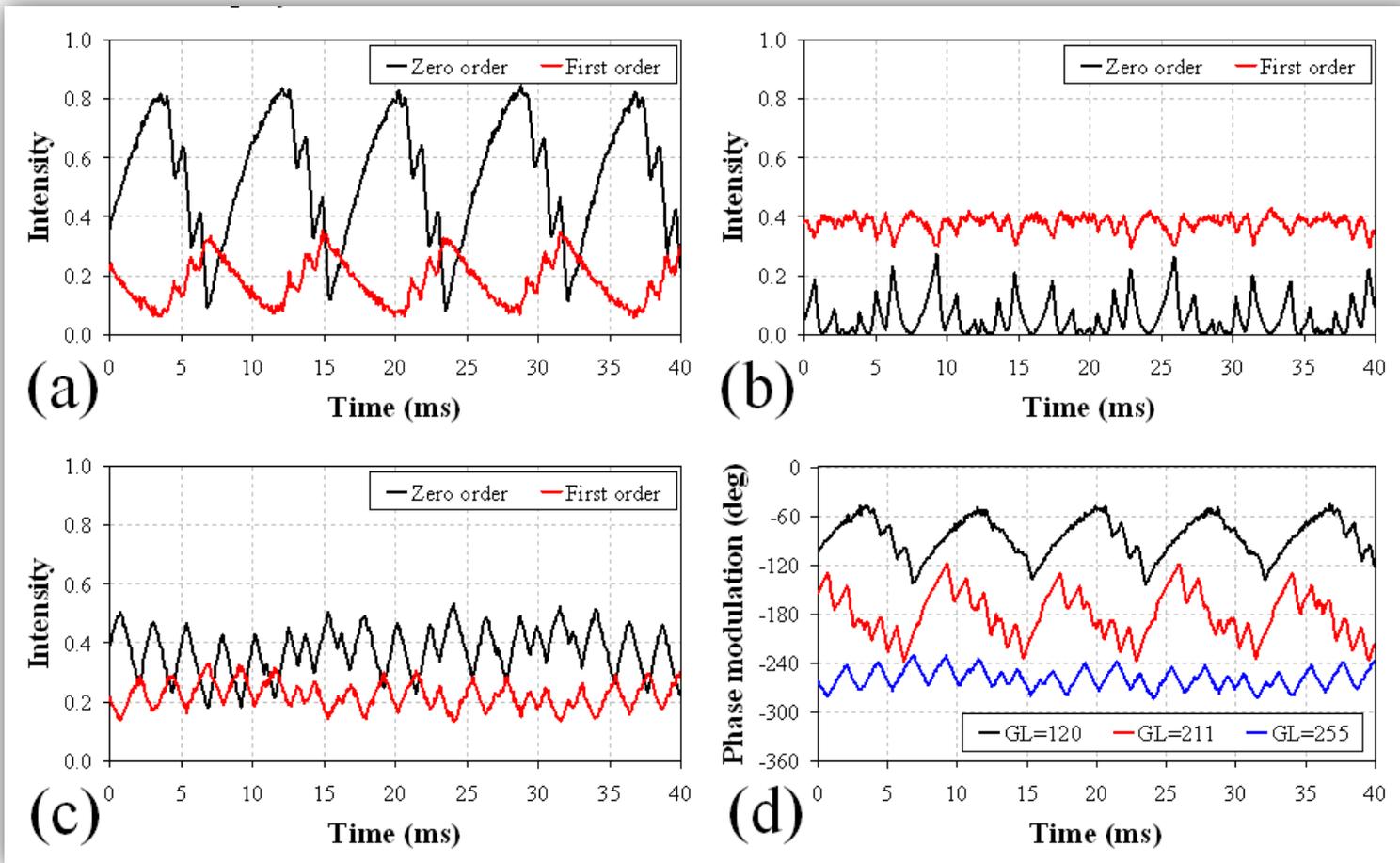


$$\cos(\Phi(t)) = \frac{4I_0(t) - \pi^2 I_1(t)}{4I_0(t) + \pi^2 I_1(t)}$$

$$\cos(\Phi_M) = \frac{4\bar{I}_0 - \pi^2 \bar{I}_1}{4\bar{I}_0 + \pi^2 \bar{I}_1} = \frac{\sin a}{a} \cos(\bar{\Phi}) \neq \cos(\bar{\Phi})$$

Phase fluctuation phenomenon

Intensity measurements at the zero and first diffraction orders for binary diffraction gratings with two different gray levels:

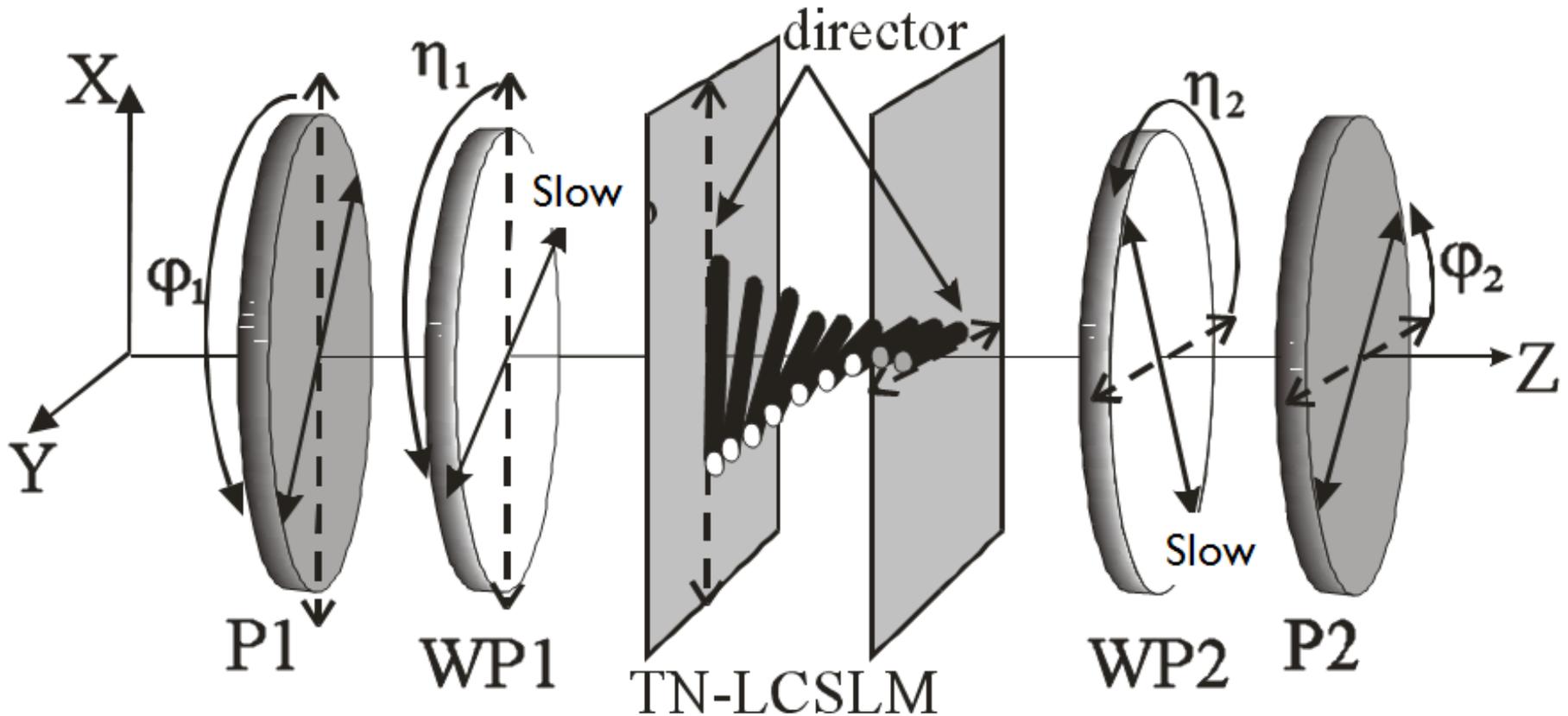


(a) (0,120), (b) (0,211) and (c) (0,255). (d) Instantaneous phase values as a function of time for different grey levels

- Polarimetric study of the liquid crystal panels

Modulation Optimization

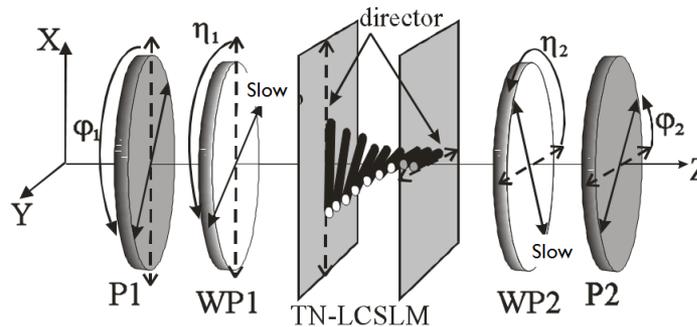
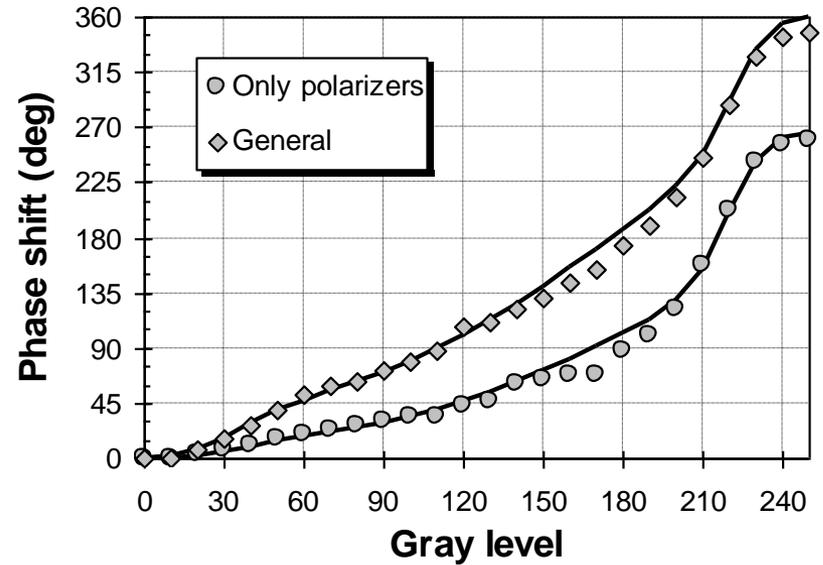
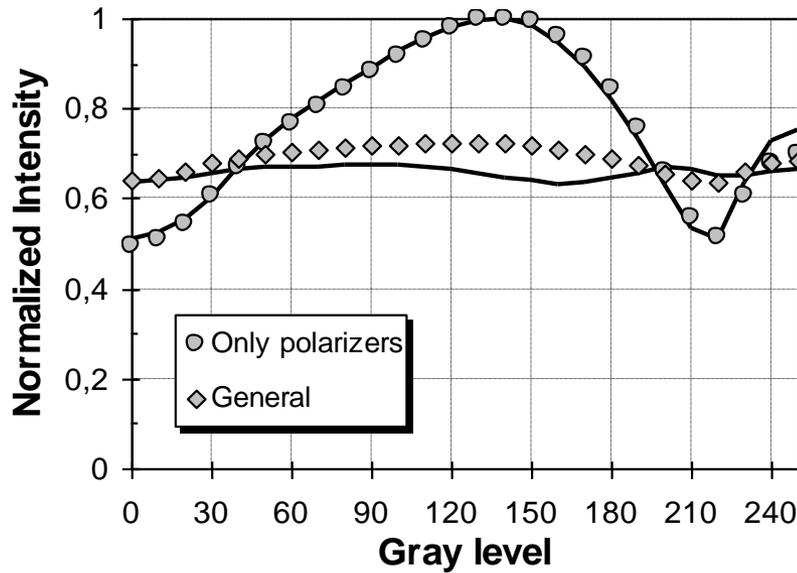
Modulation Optimization



Modulation Optimization



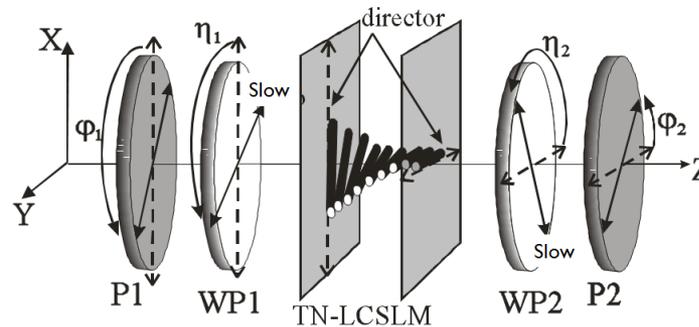
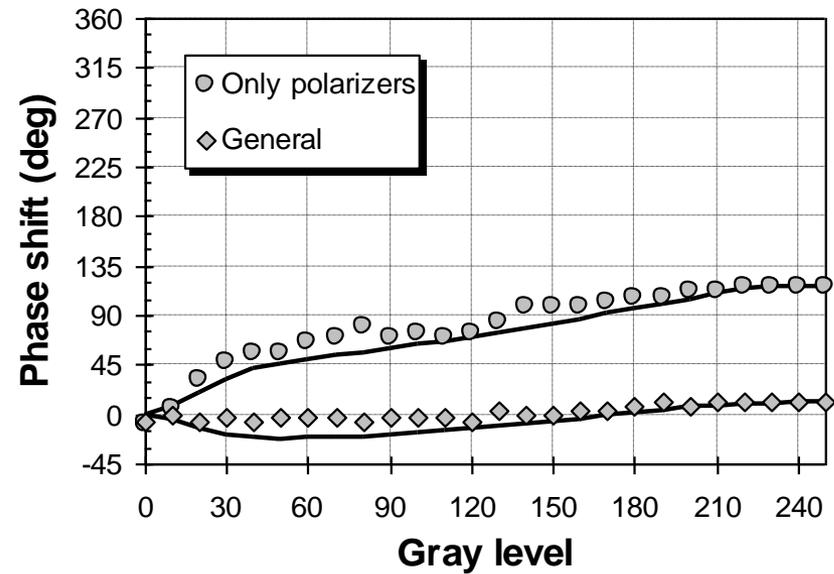
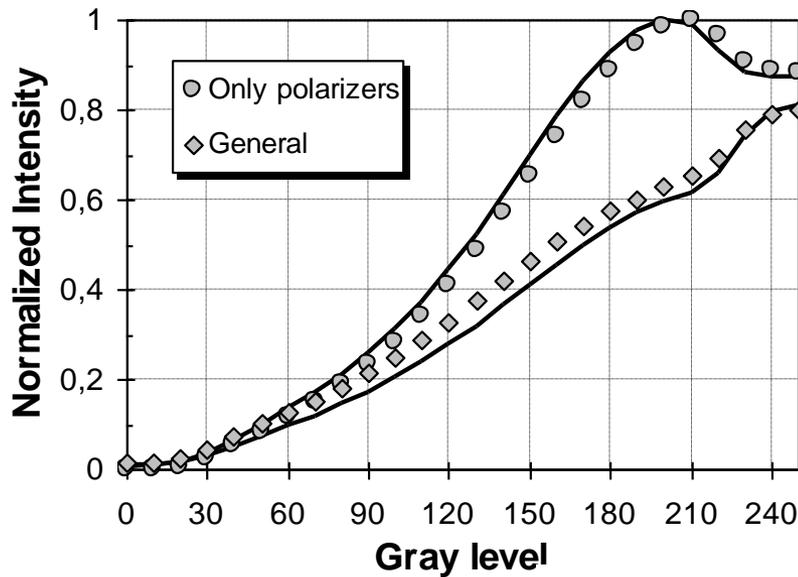
- Phase-only modulation



Modulation Optimization

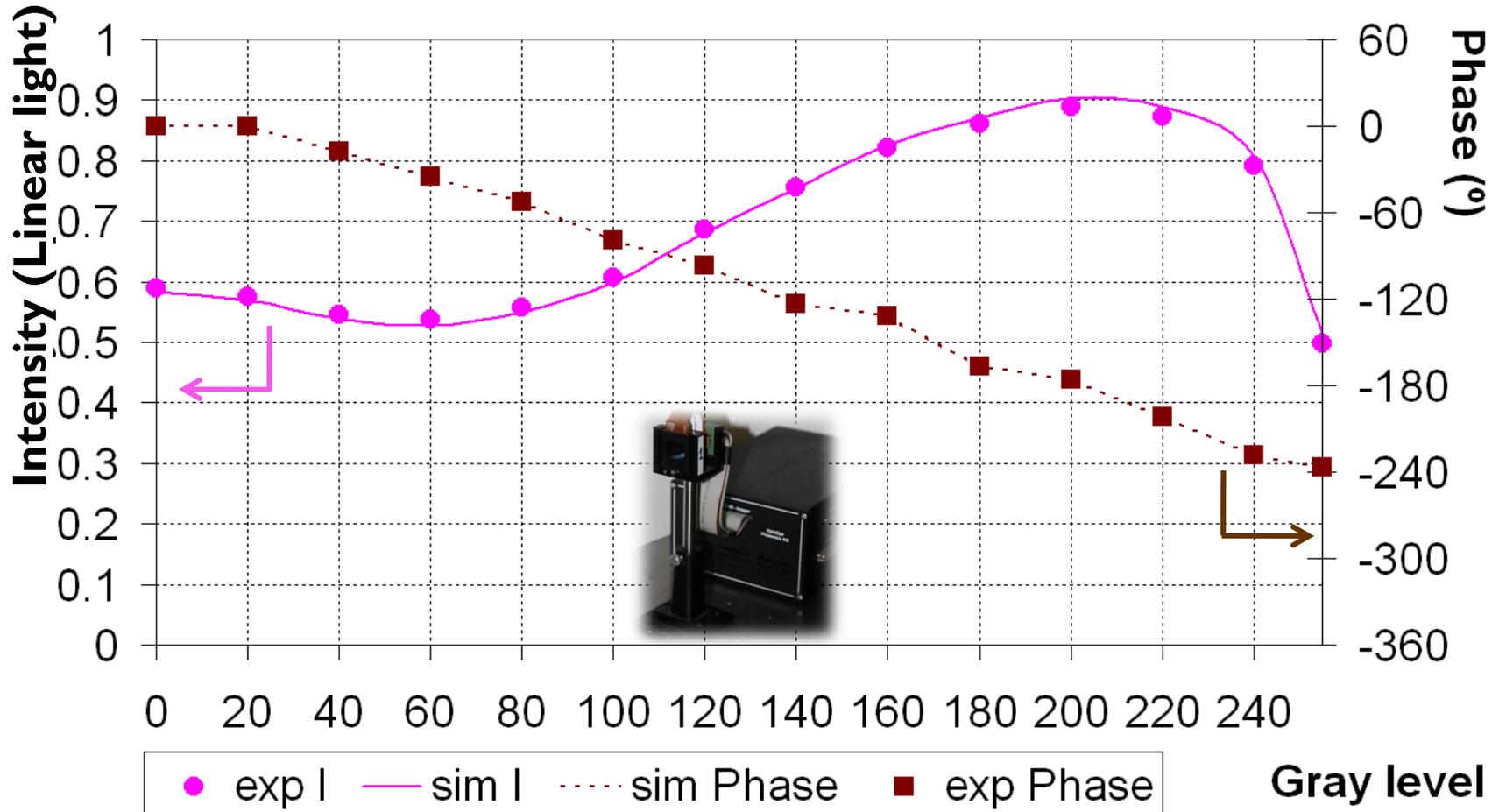


• Amplitude-only modulation



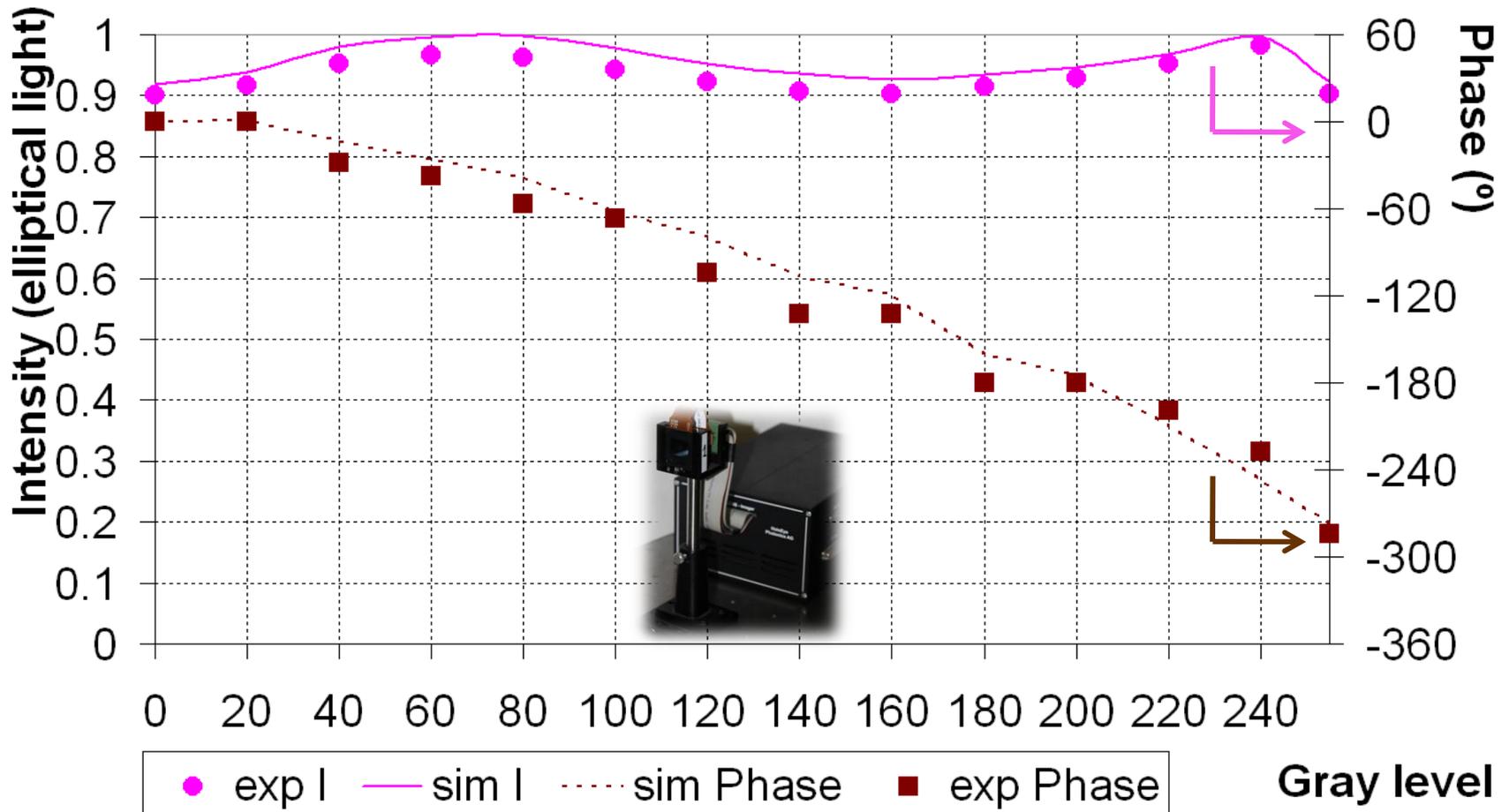
LCoS display response optimization

Optimized results for : 633 nm; Only polarizers and 2° incident angle.



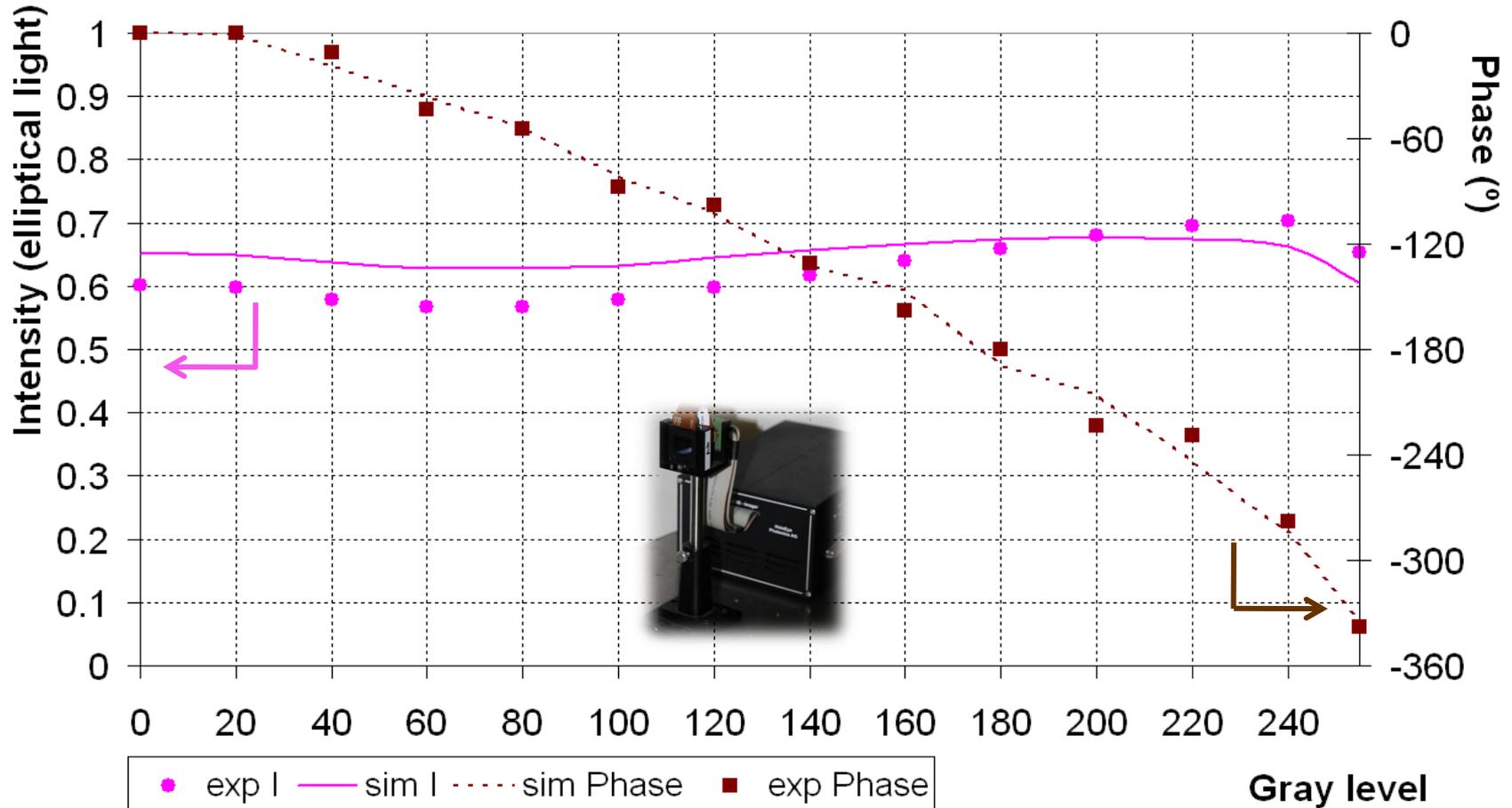
LCoS display response optimization

Optimized results for : 633 nm; Polarizers and Wave plates and 2° incident angle.

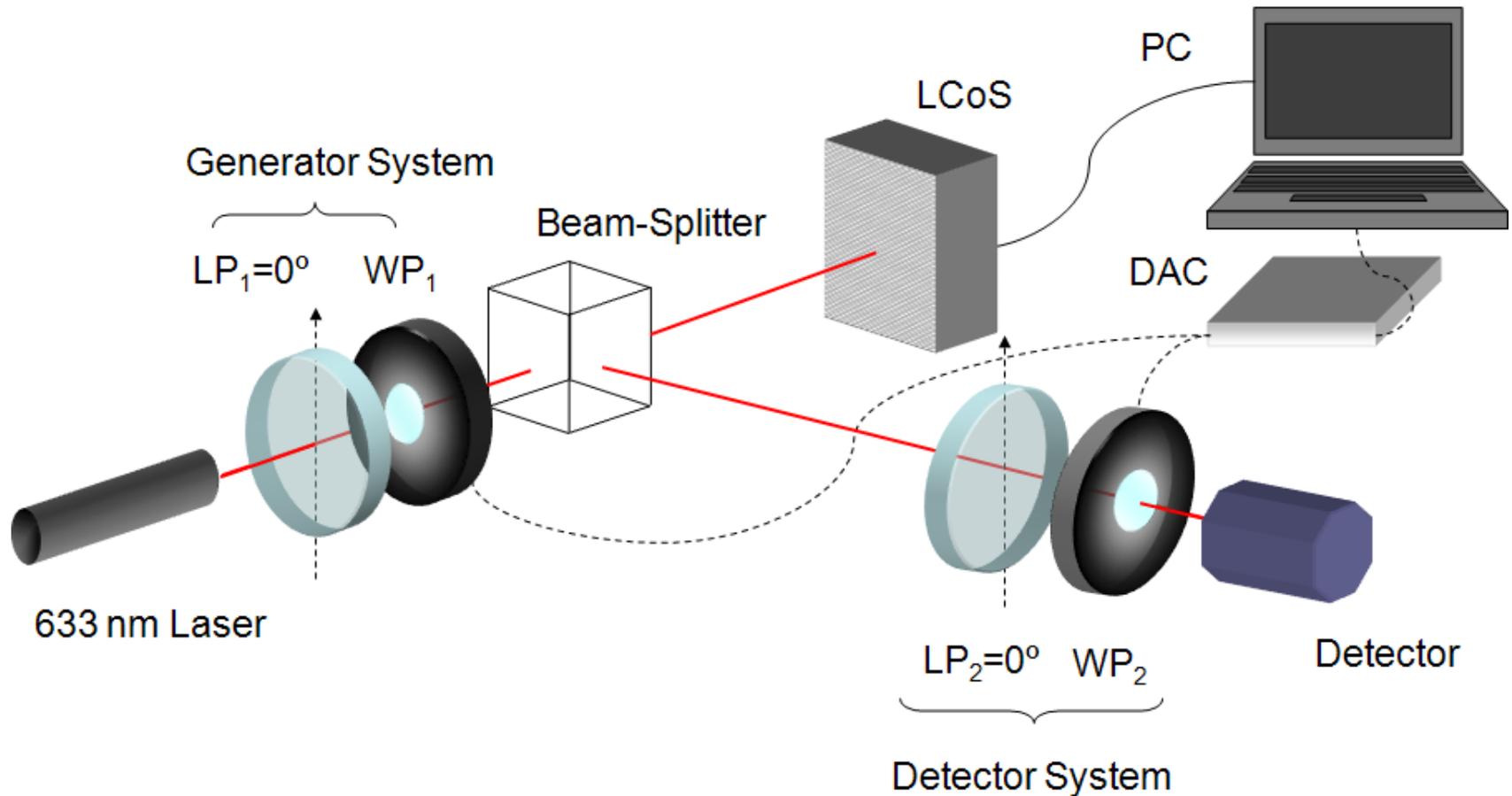


LCoS display response optimization

Optimized results for : 633 nm; Polarizers and Wave plates and 2° incident angle.



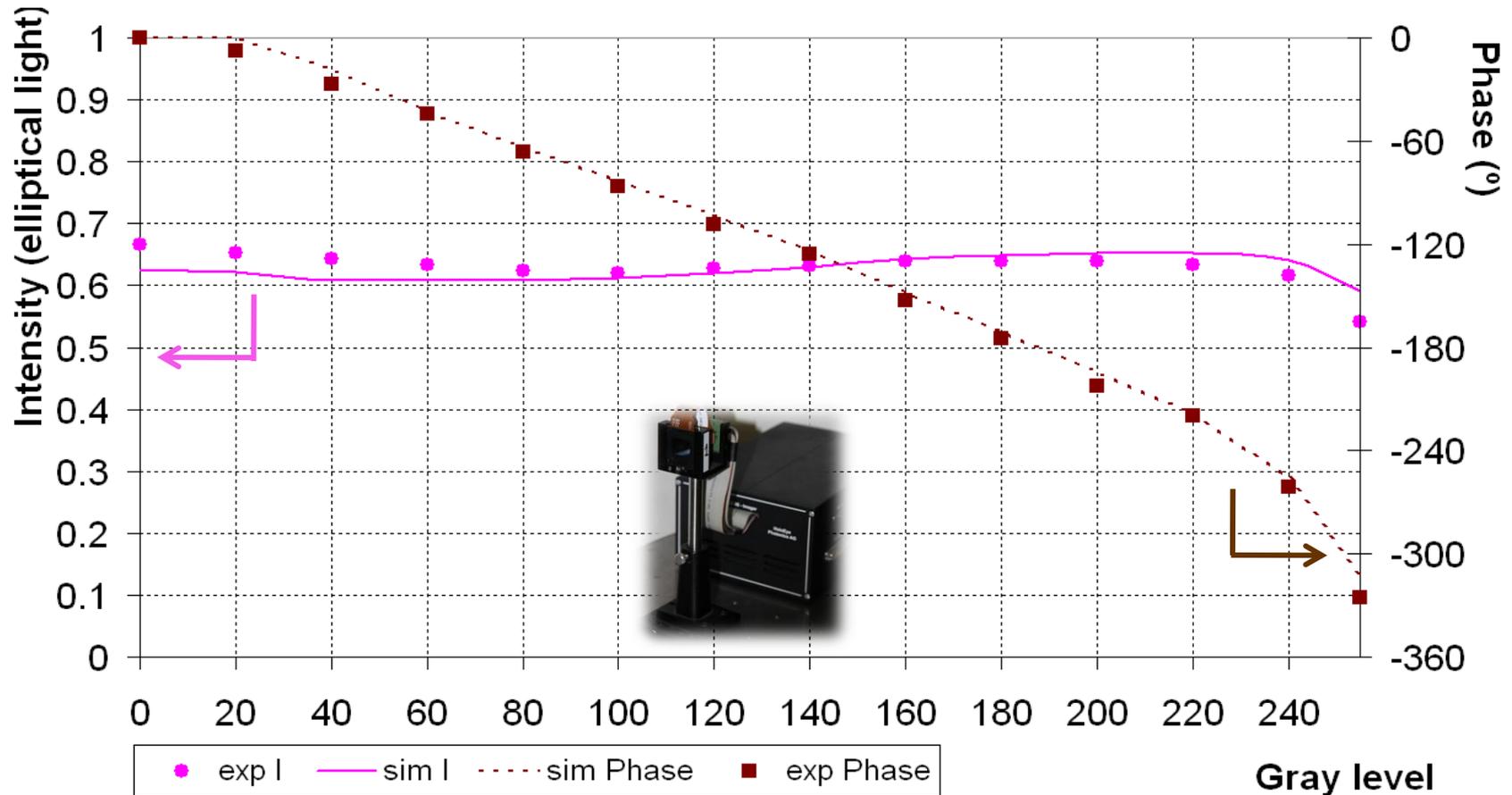
LCoS display response optimization



 **Beam-splitter based set-up.**

LCoS display response optimization

Optimized results for : 633 nm; Polarizers and Wave plates and Beam-splitter.

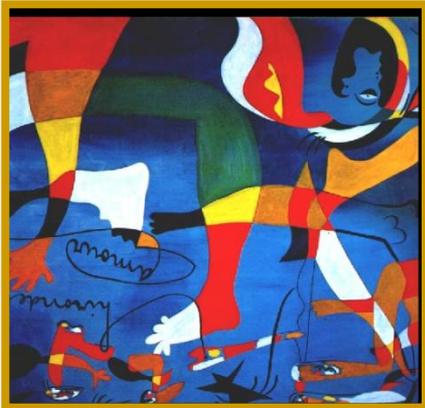


Use of commercial LCDs in diffractive Optics

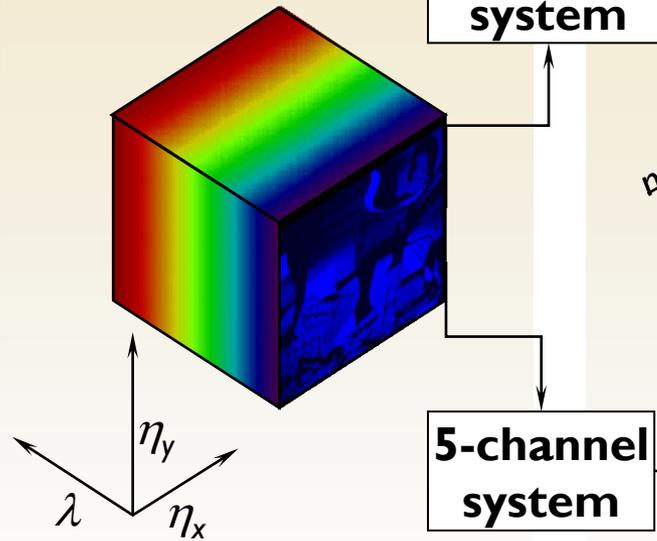
Pattern recognition

Color Pattern Recognition

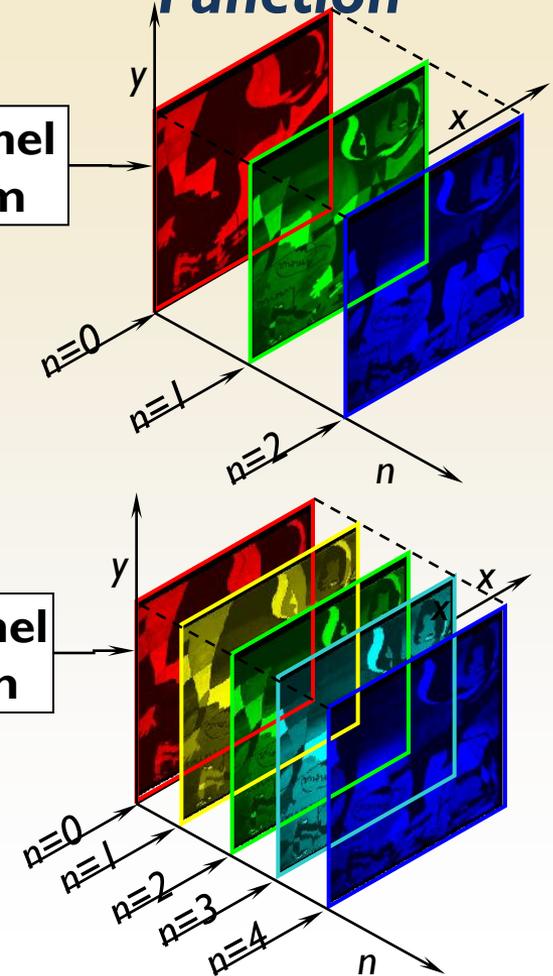
Color Image



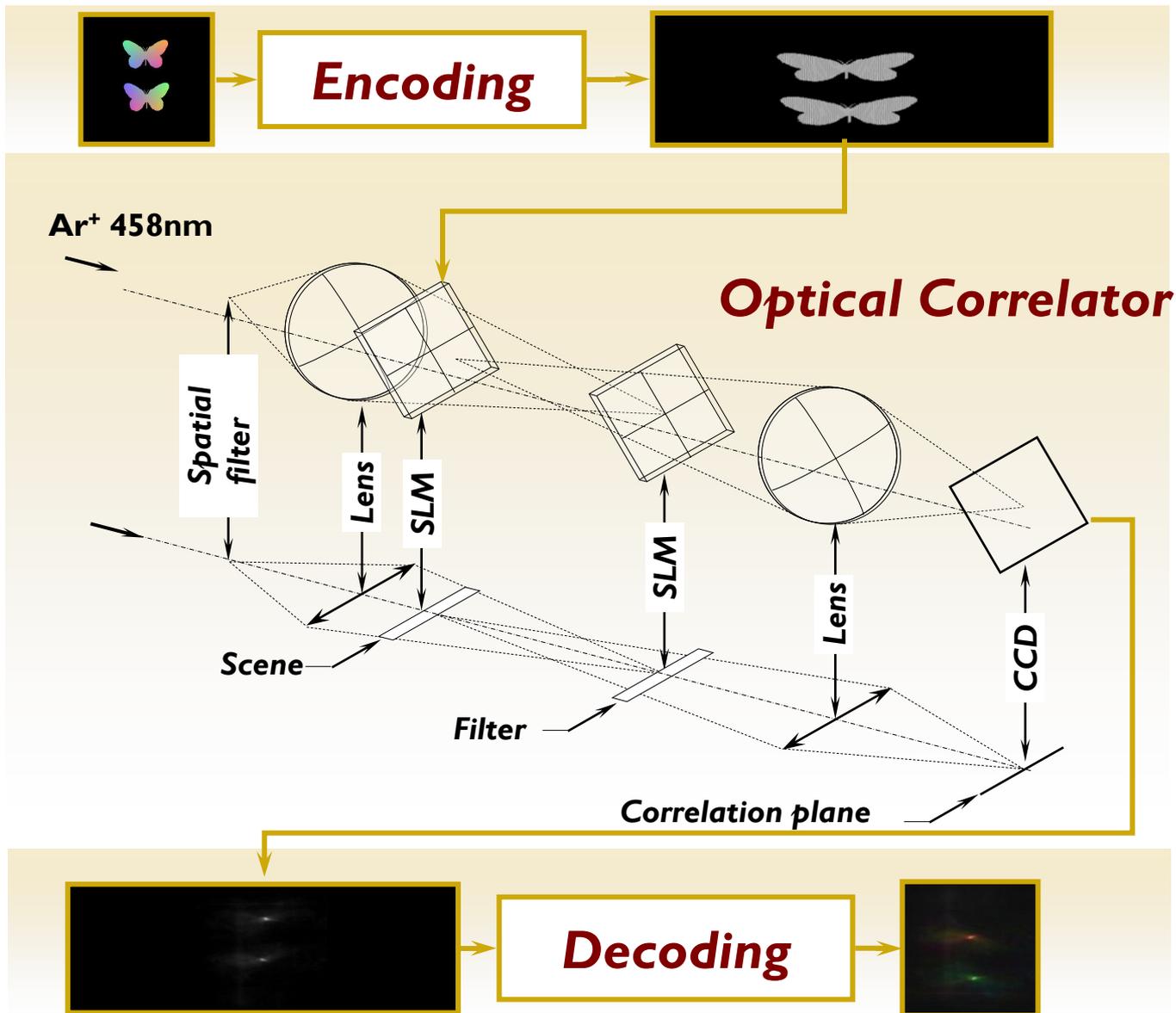
3D Continuous Function



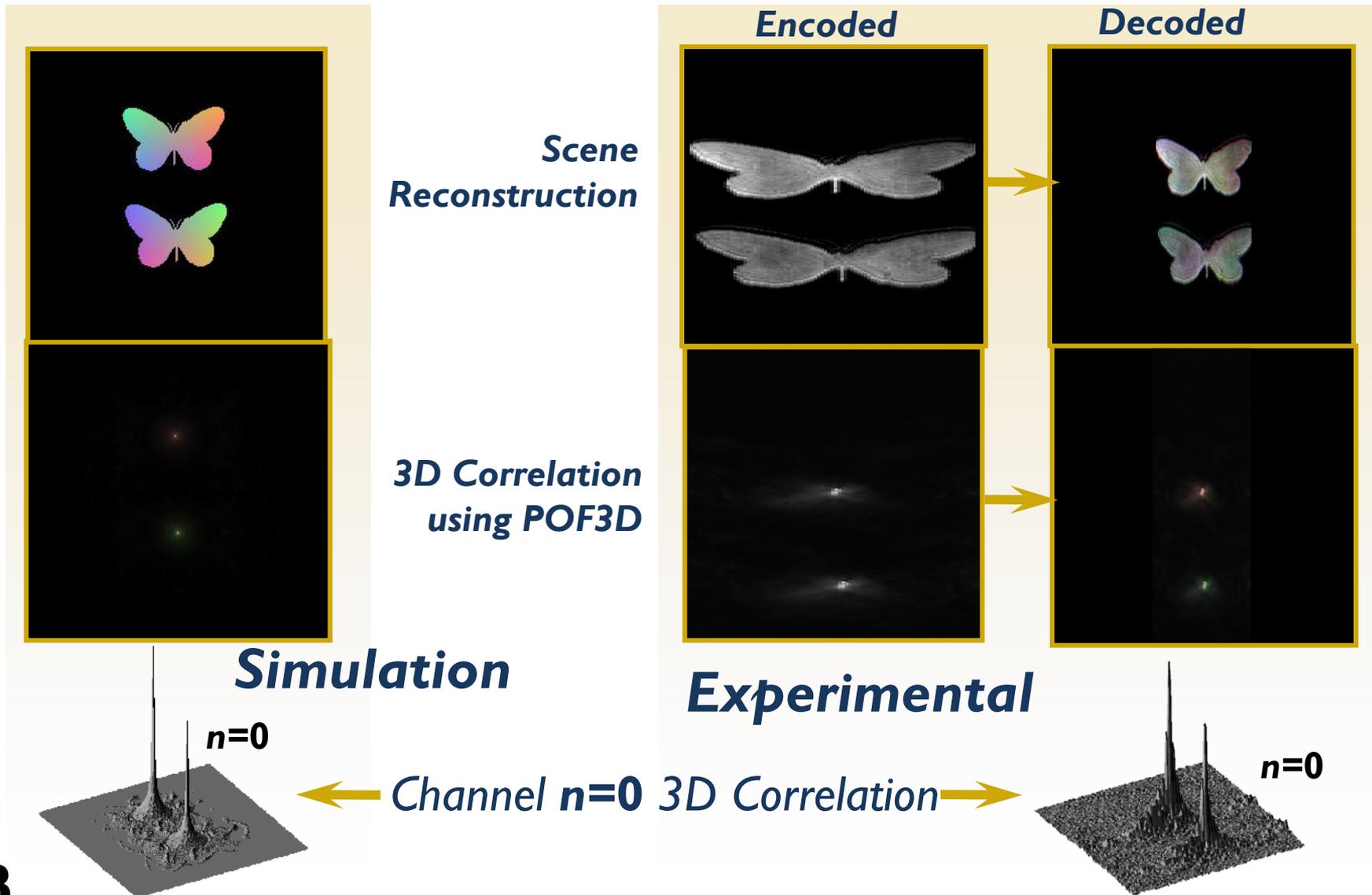
3D Sampled Function



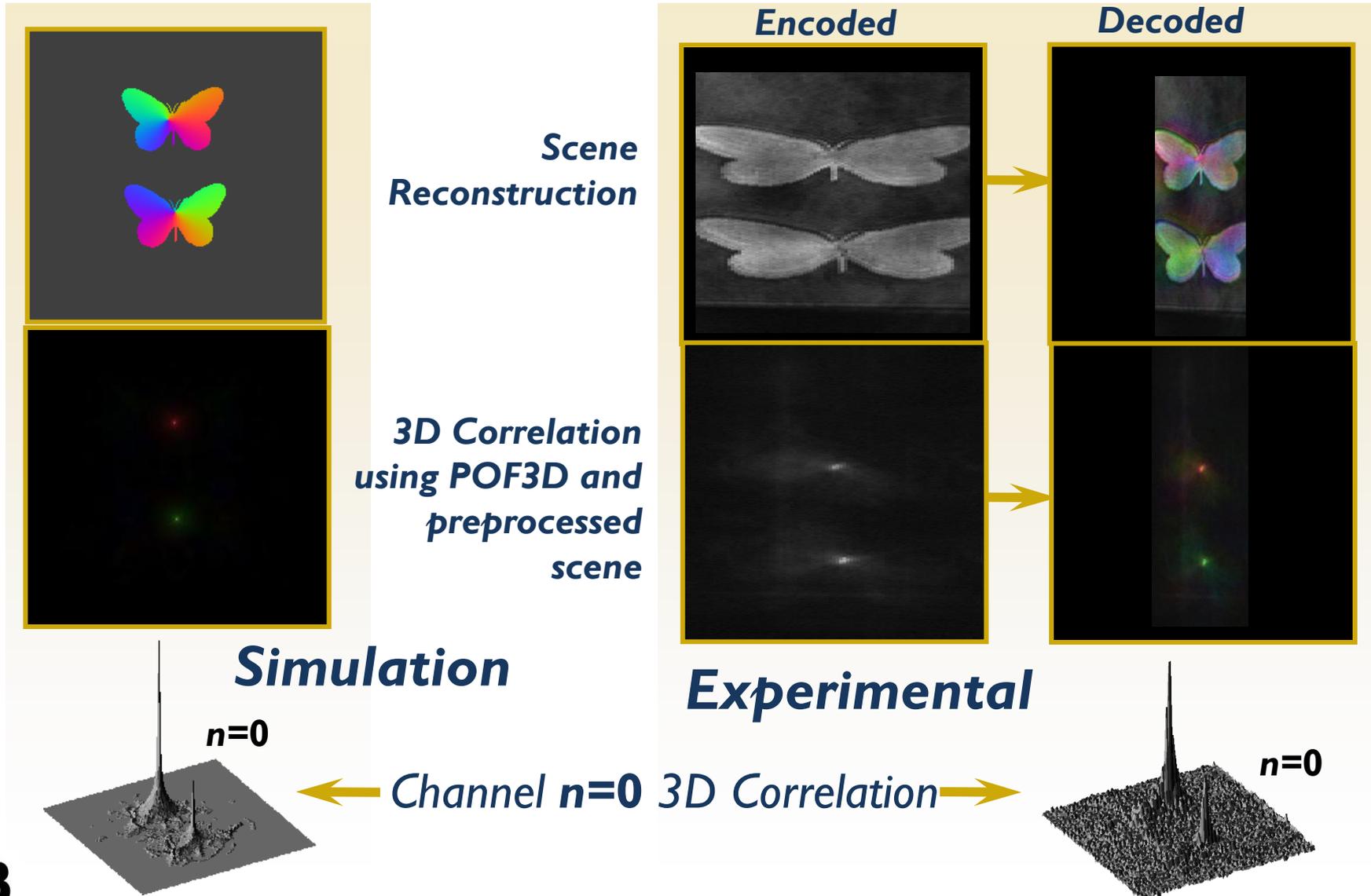
Color Pattern Recognition



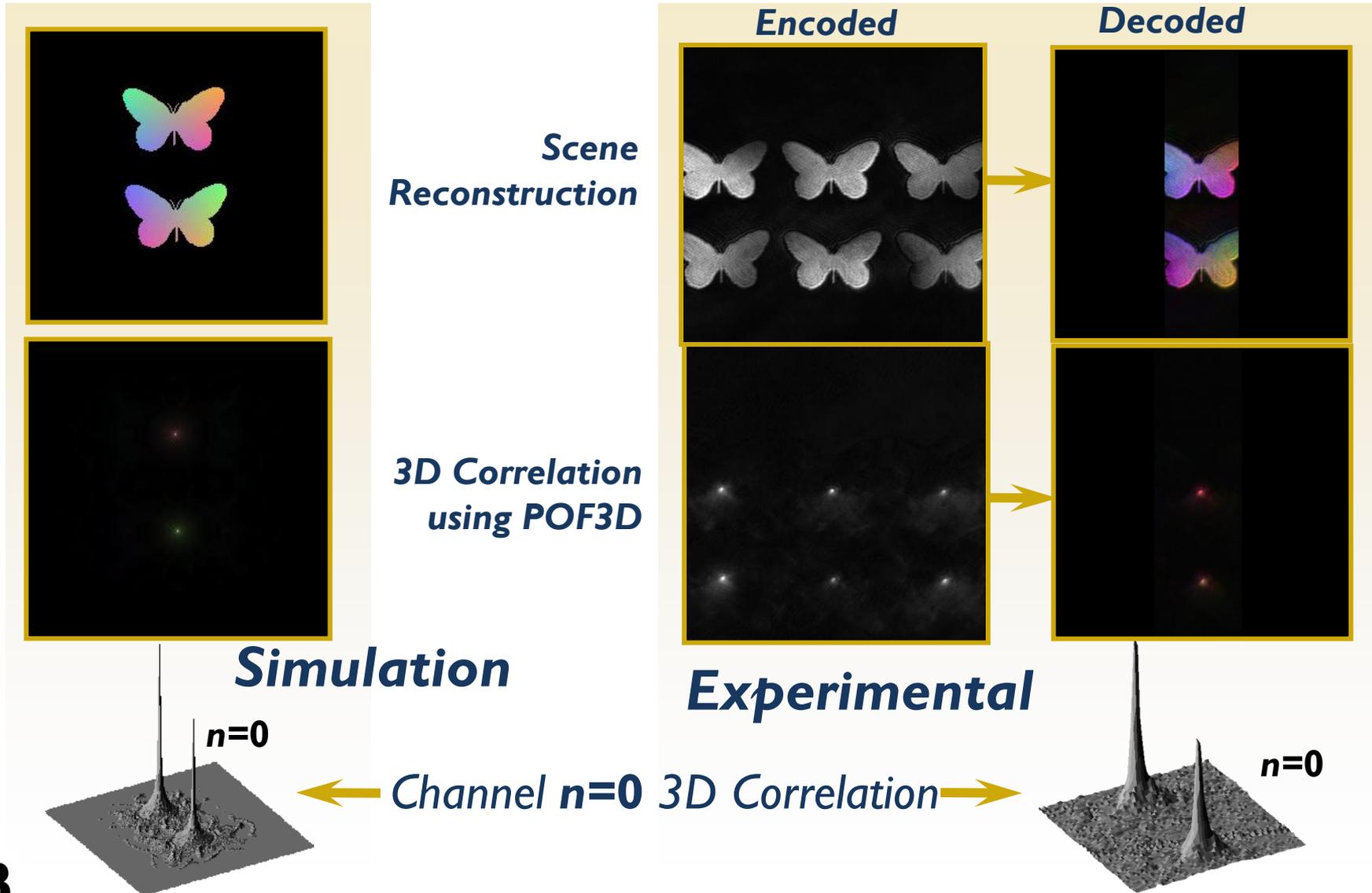
Color Pattern Recognition



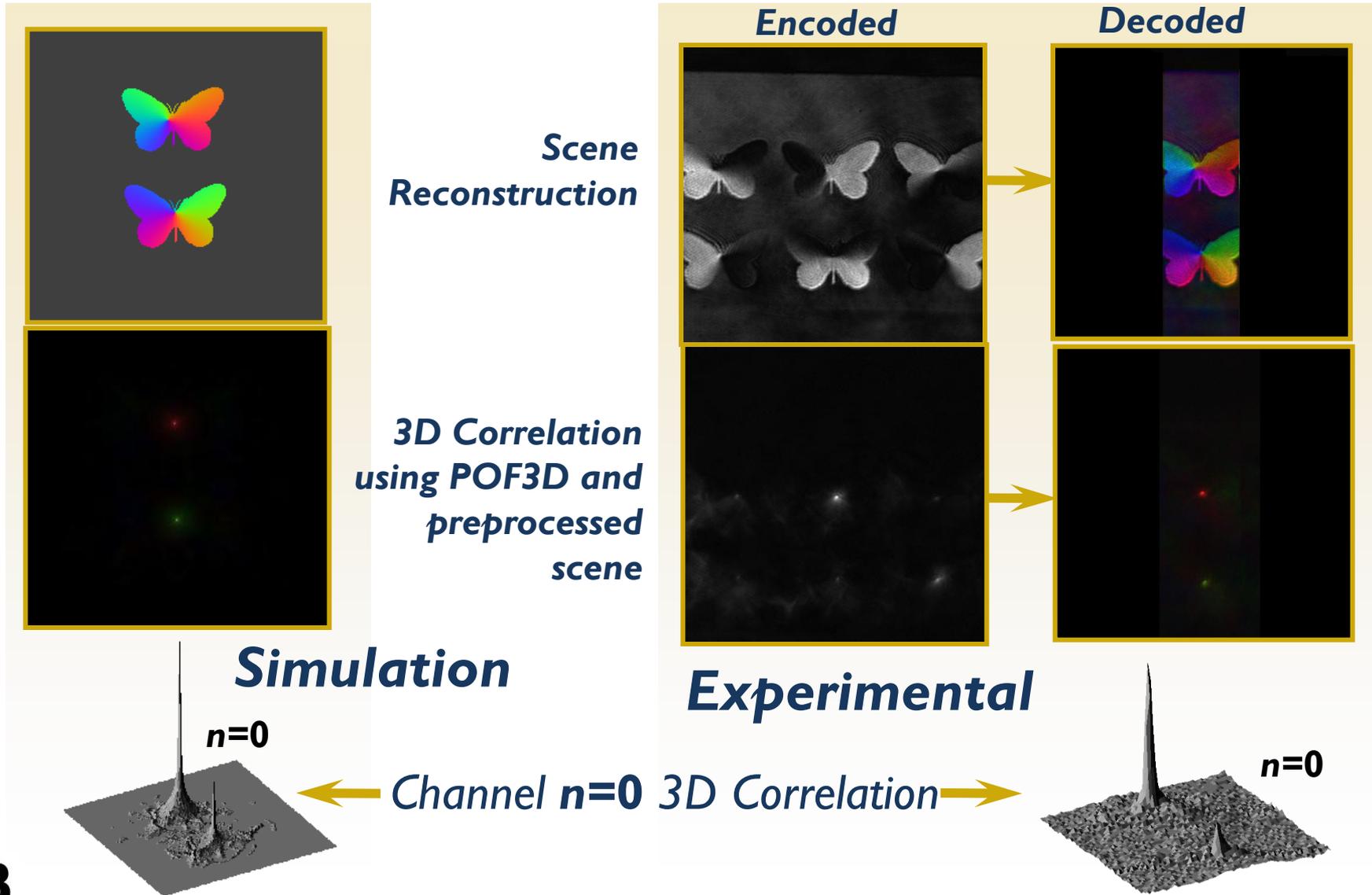
Color Pattern Recognition



Color Pattern Recognition



Color Pattern Recognition



Use of commercial LCDs in diffractive Optics

Apodizing filters

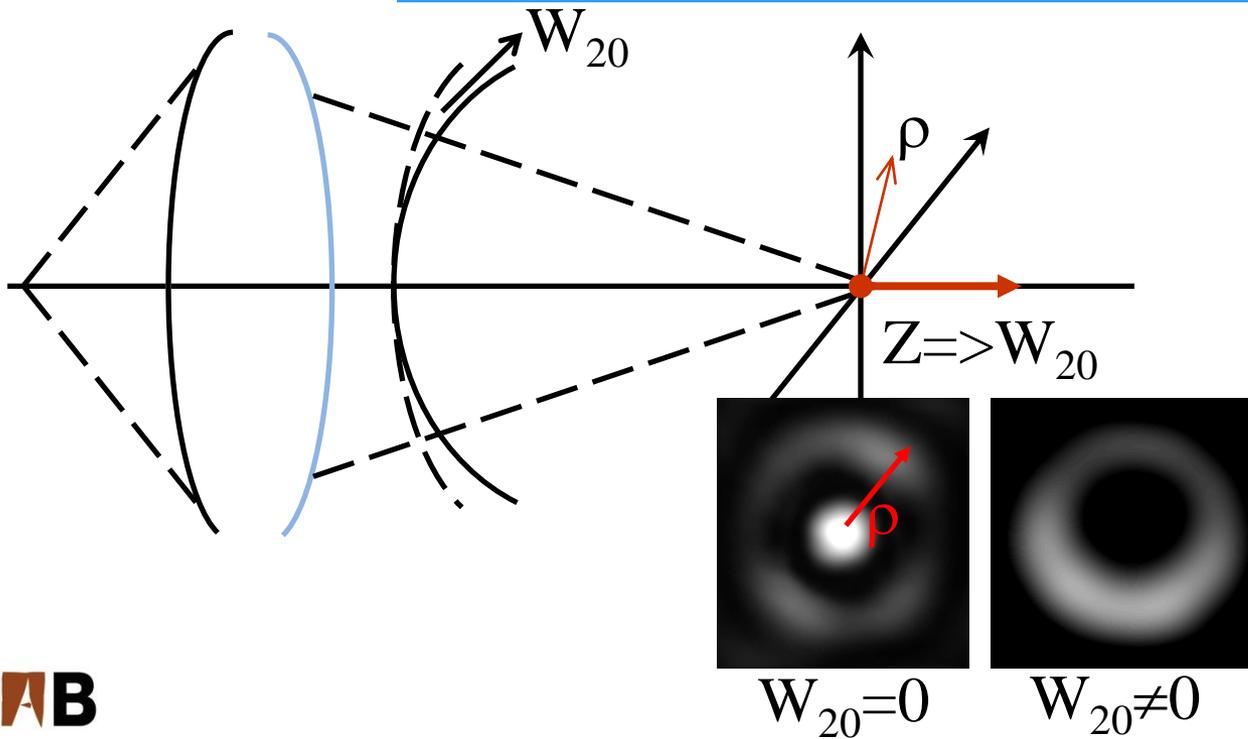
Apodizing filters

The **3-D Point Spread Function** (PSF) of an optical system is given by:

$$G(\rho, W_{20}) = \left(1/\lambda^2\right) \left|F_{\lambda}(\rho, W_{20})\right|^2$$

$F_{\lambda}(\rho, W_{20})$ **monochromatic amplitude** (optical system with radial symmetry) :

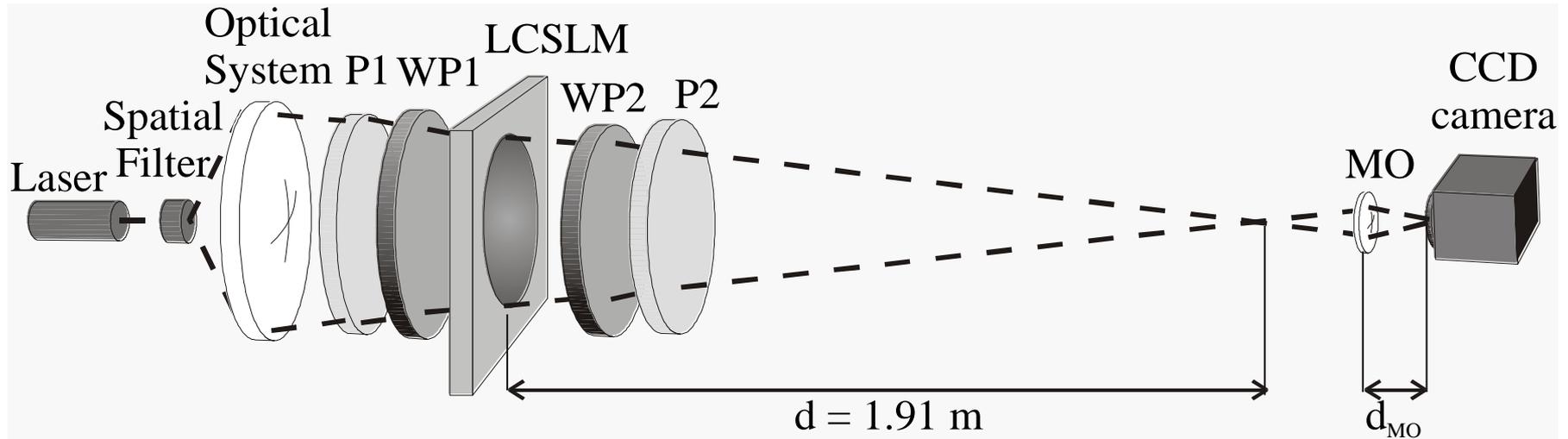
$$F_{\lambda}(\rho, W_{20}) = 2\pi \int_0^1 t(r) \exp[i2\pi W_{20}r^2] J_0(2\pi\rho r) r dr$$



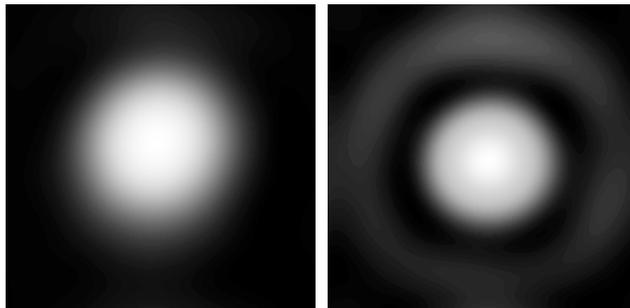
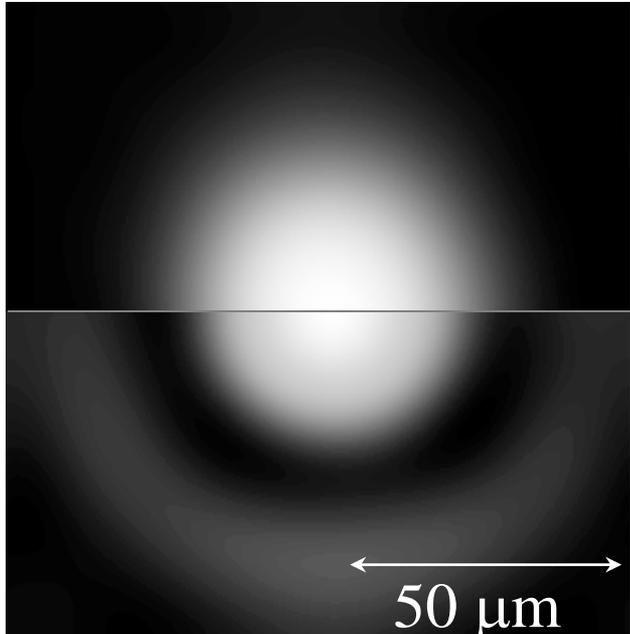
$$s = \frac{\lambda}{NA} \rho$$

$$z = \frac{2\lambda}{NA^2} W_{20}$$

Apodizing filters



$$\tau(r) = 1 - r^2 \text{ and } \tau(r) = r^2$$



$t(r) = 1 - r^2$ (transverse response)				
Position	ρ' (μm) (theory)	Intensity N2	ρ' (μm) (exper)	Intensity N2
Center	0	1	0	1
1 ^{rst} min.	84.1	0	88.3	0
1 ^{rst} max.	105.9	0.004	---	---

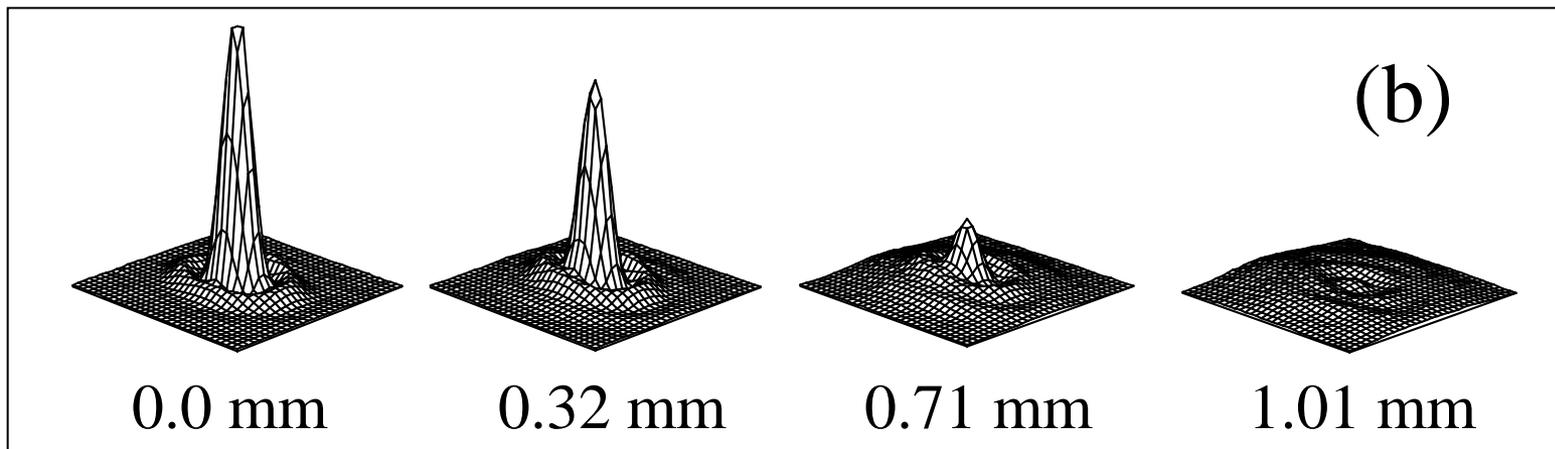
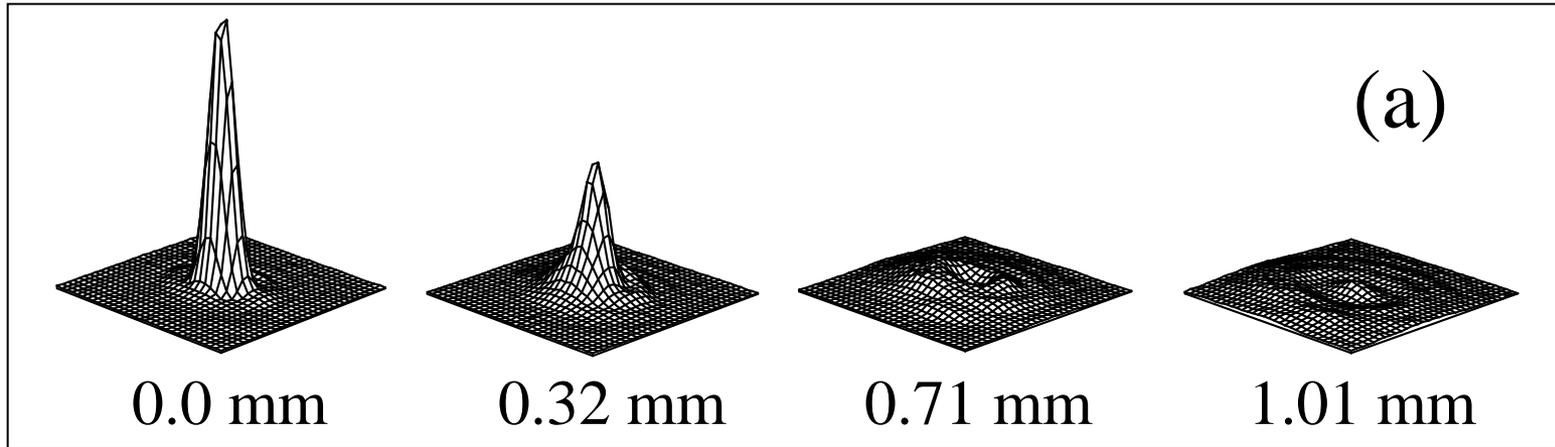
$t(r) = r^2$ (transverse response)				
Position	ρ' (μm) (theory)	Intensity N2	ρ' (μm) (exper)	Intensity N2
Center	0	1	0	1
1 ^{rst} min.	49.8	0	54.3	0
1 ^{rst} max.	74.7	0.08	79.9	0.07

$$\tau(r) = 1 - r^2$$

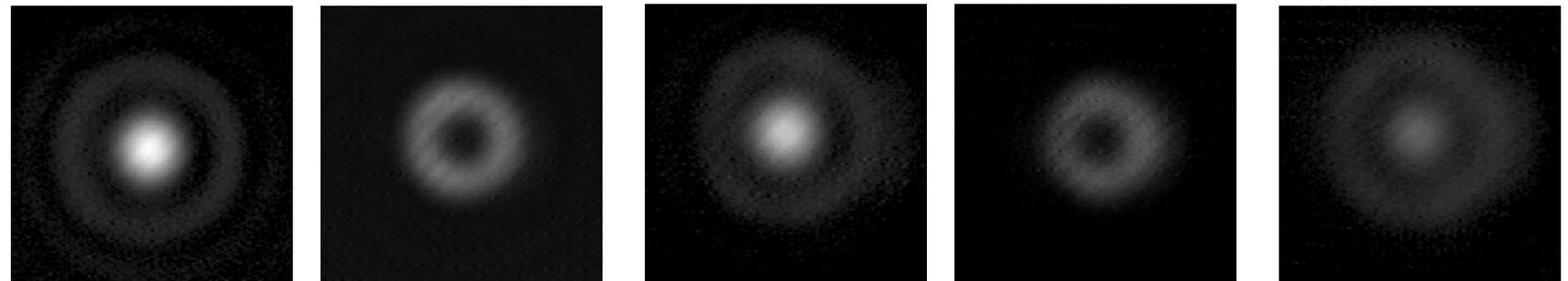
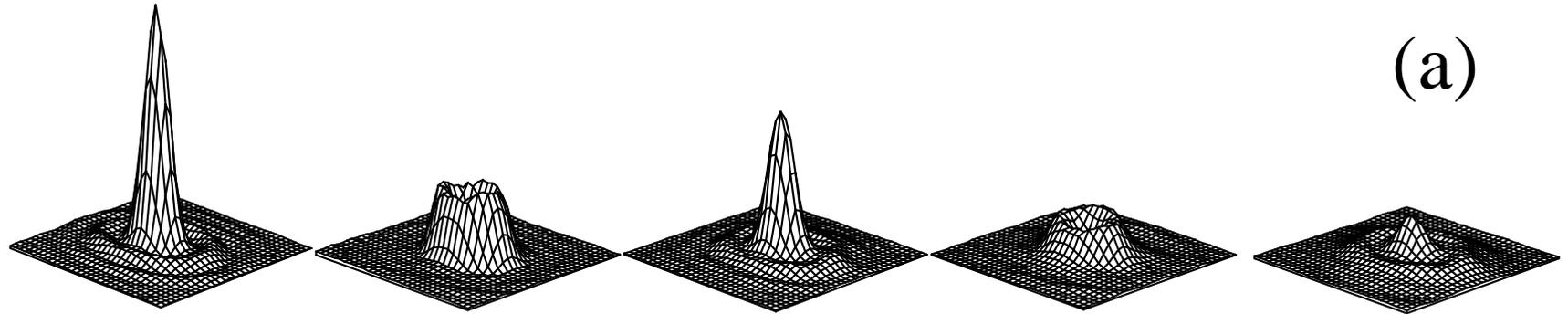
$$\tau(r) = r^2$$

Clear aperture

Axial apodizing filter: $\tau(r) = 6.75 r^2 - 13.5 r^4 + 6.75 r^6$



Axial hyperresolving filter: $\tau(r) = 1 - 4r^2 + 4r$



0.0 mm

0.47 mm

0.88 mm

1.32 mm

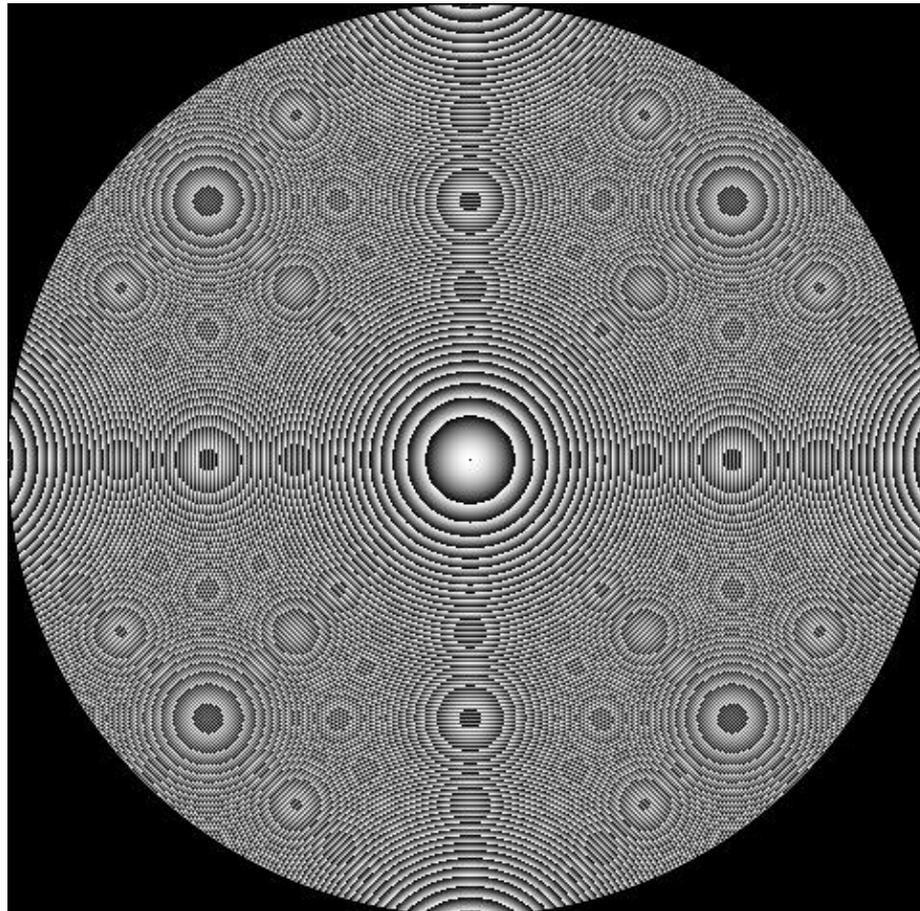
1.69 mm

Use of commercial LCDs in diffractive Optics

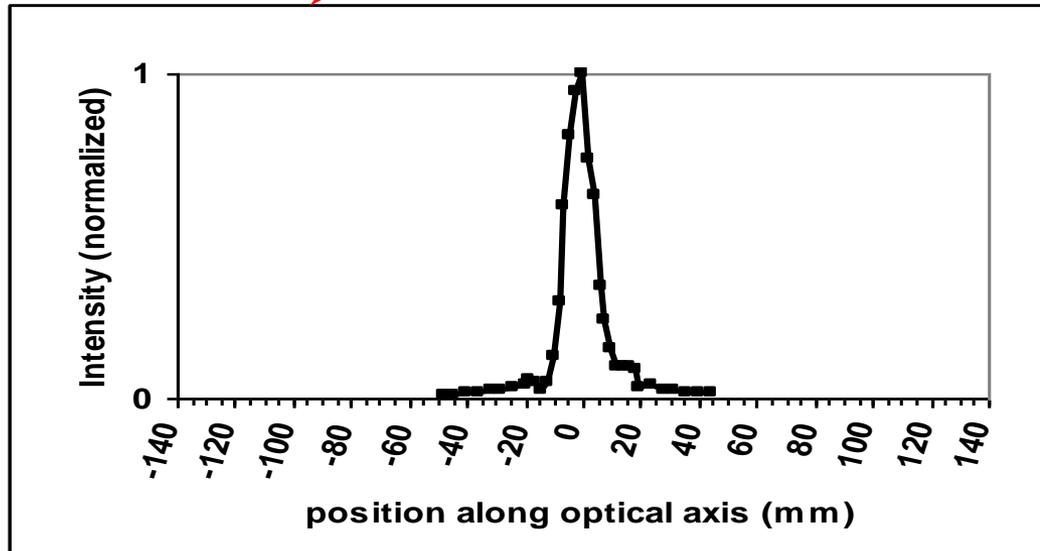
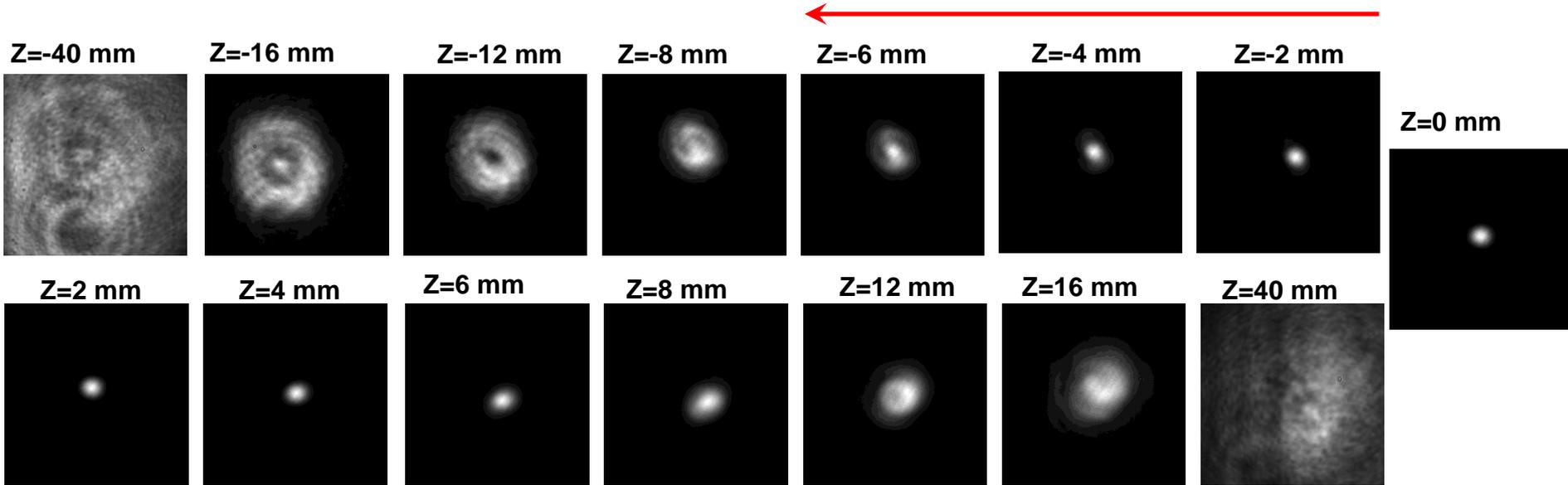
Multiplexed lenses

Single lens

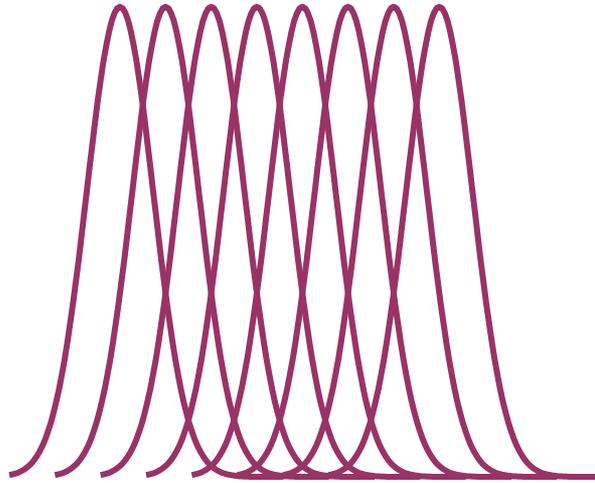
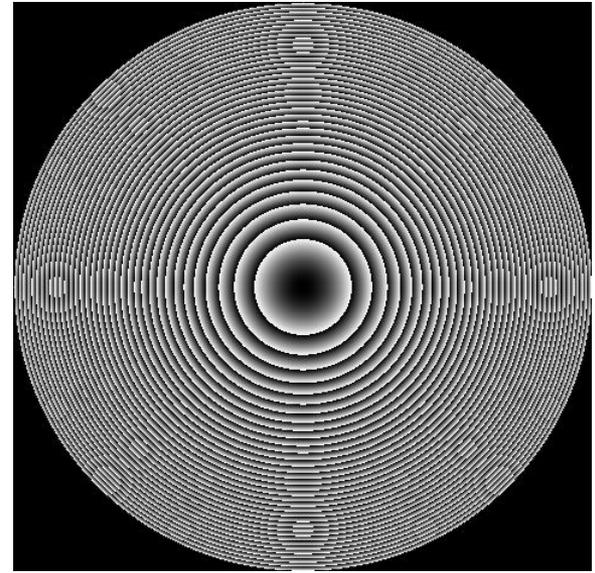
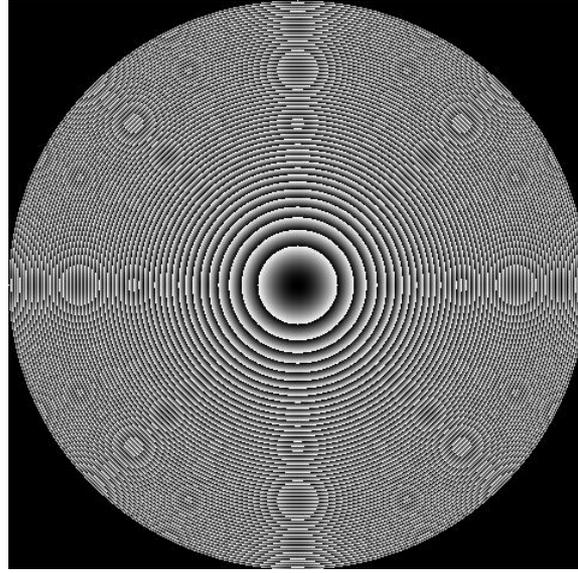
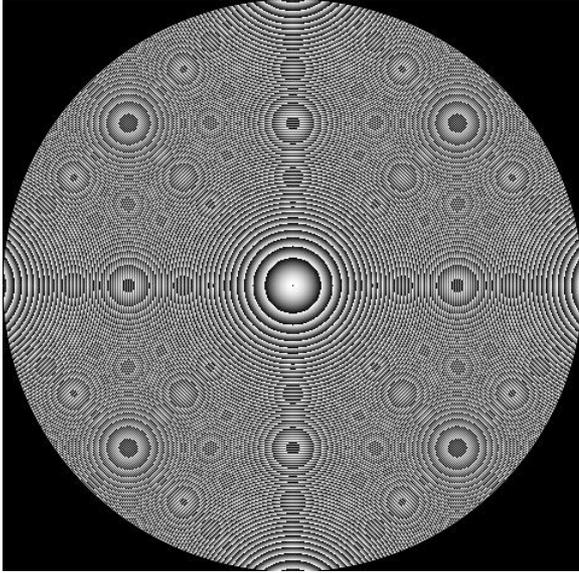
- Lens with a focal length of 1000 mm for the blue line of an Ar laser ($\lambda = 458 \text{ nm}$)



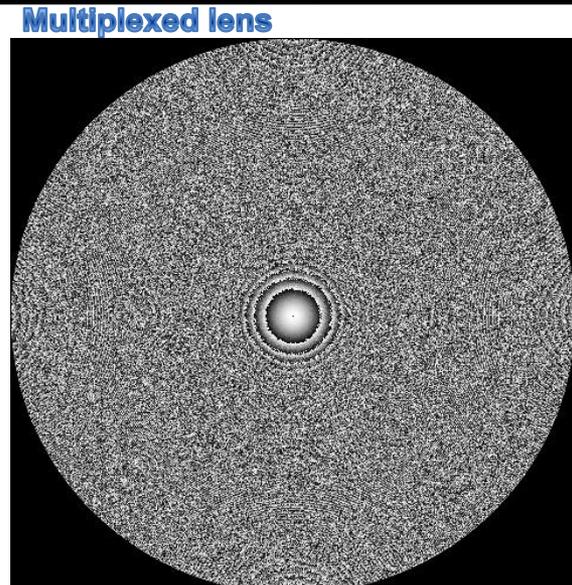
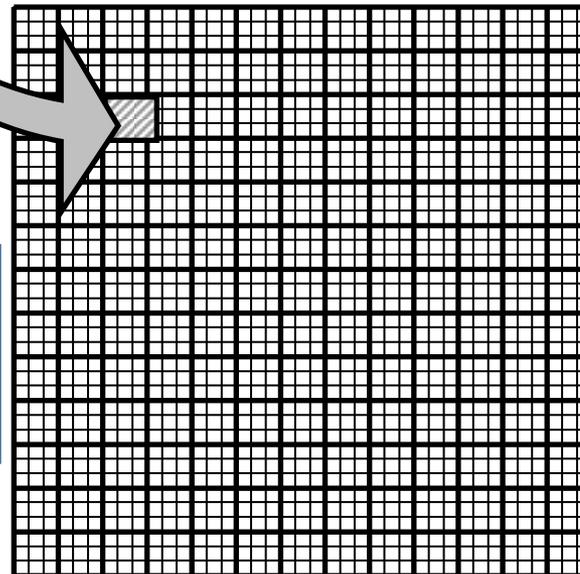
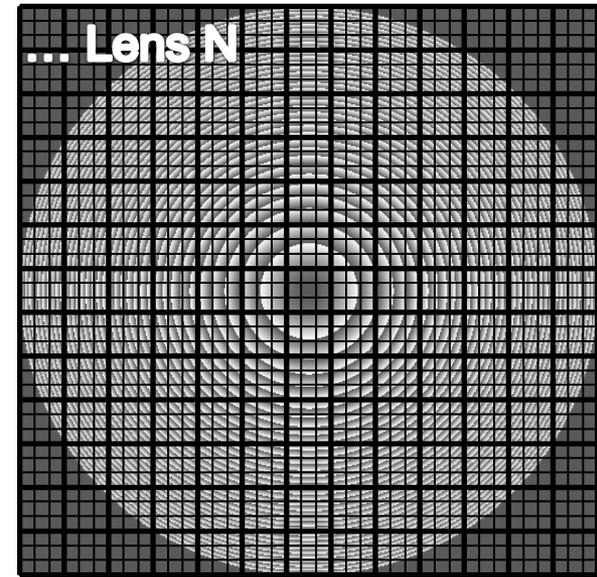
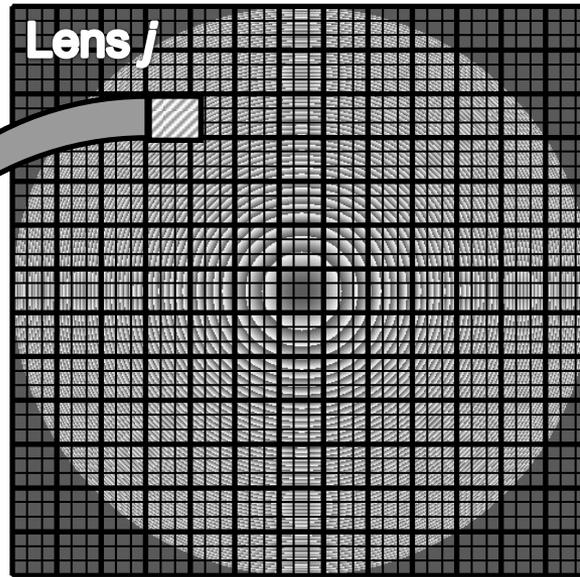
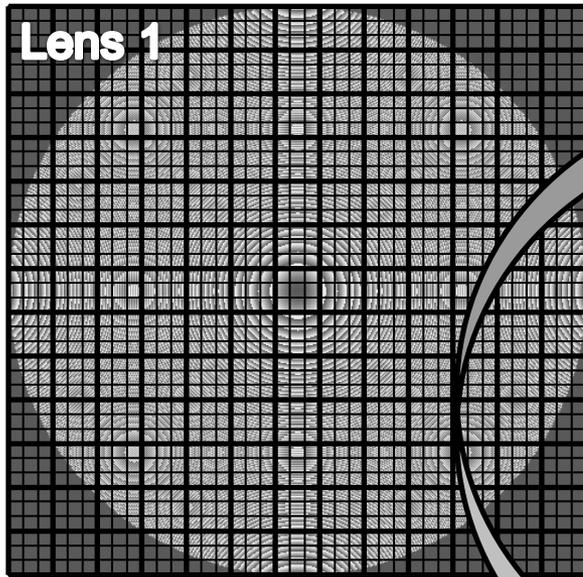
Single lens



Multiplexed Lens



Randomly multiplexed lenses

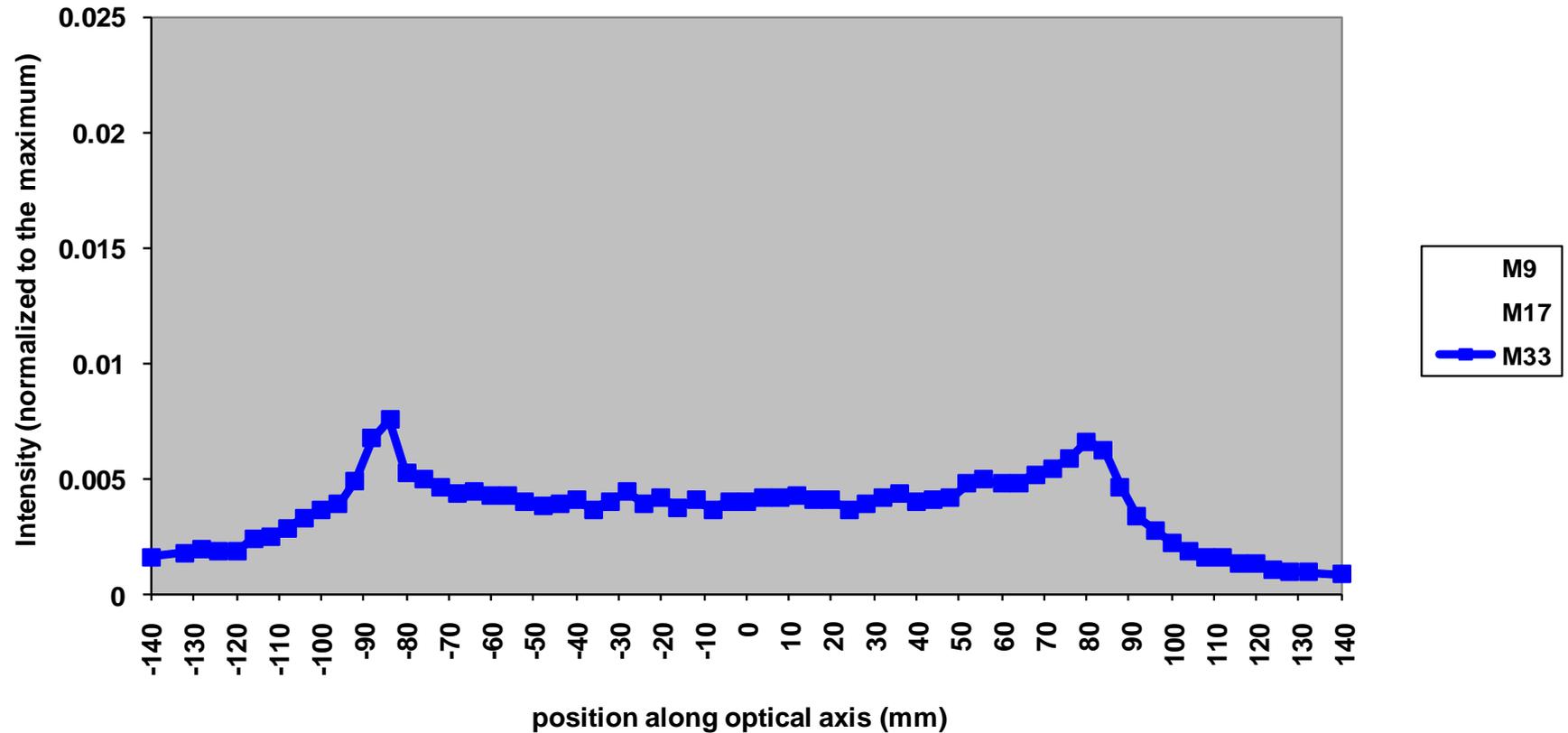


N: Number of lenses
P: Number of pixels for each lens

K random number (0,N]

$$j-1 < K \leq j$$

Randomly multiplexed 33 lenses



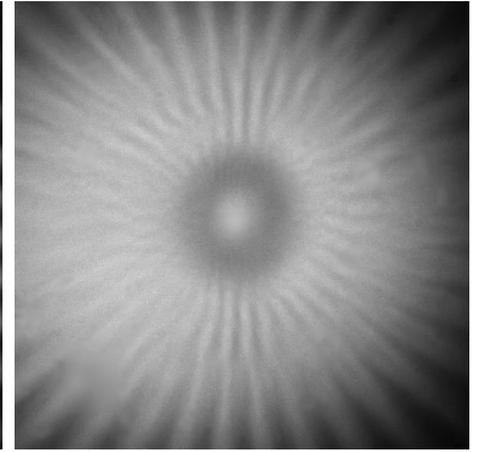
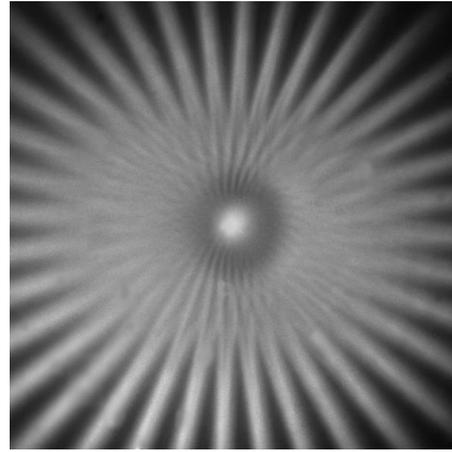
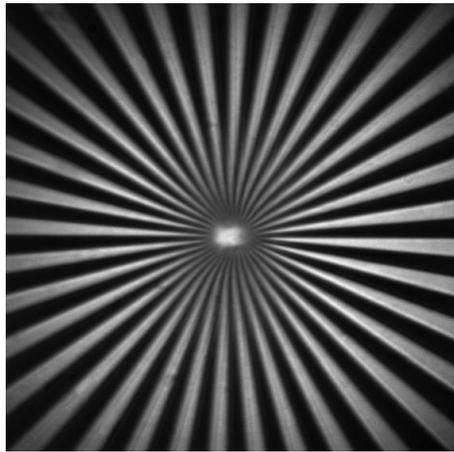
Randomly multiplexed 33 lenses

Z = 0 cm.

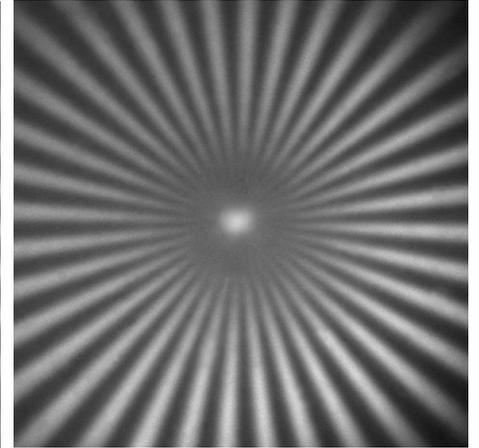
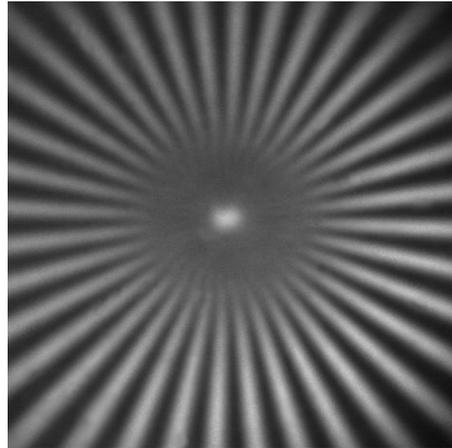
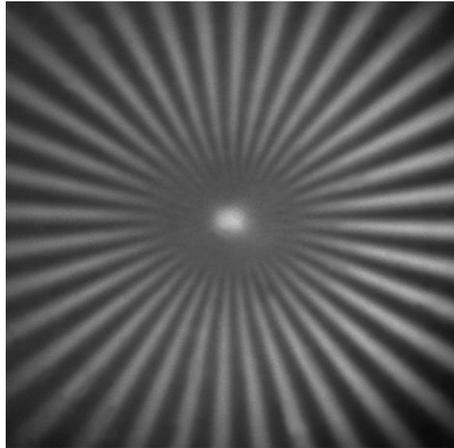
Z = -6 cm.

Z = -10 cm.

Single lens



Multiplexed lens



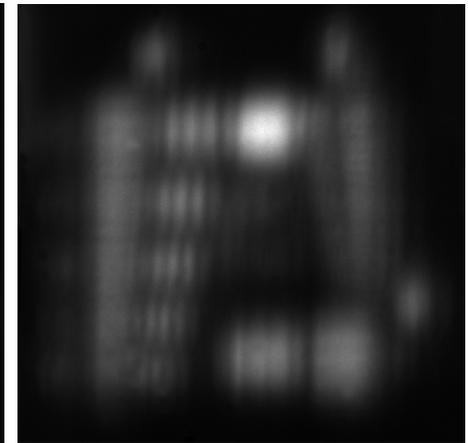
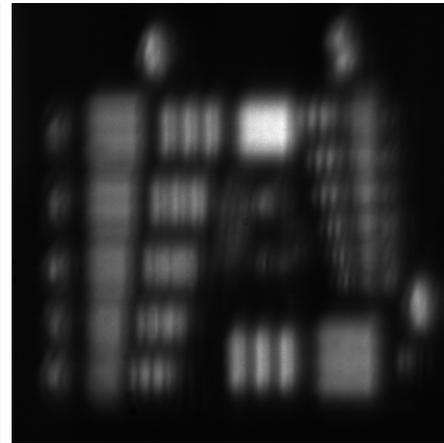
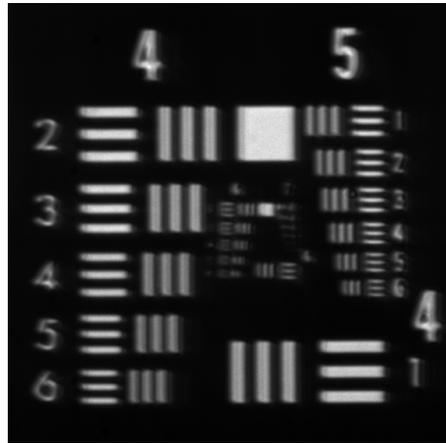
Randomly multiplexed 33 lenses

Z = 0 cm.

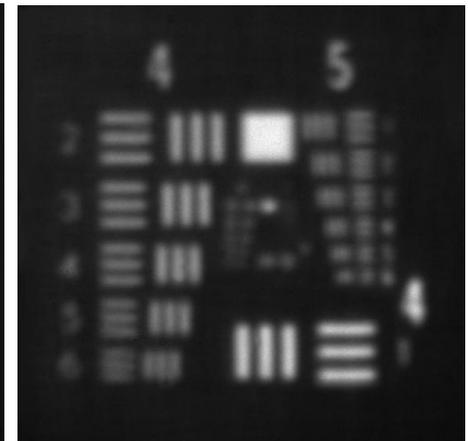
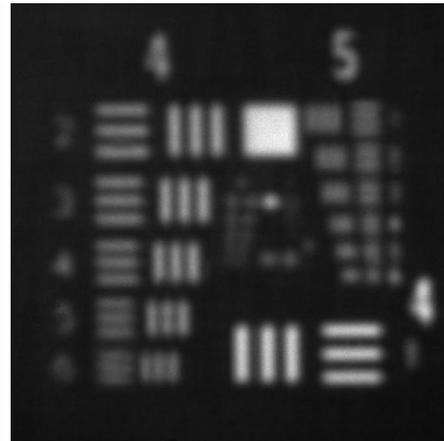
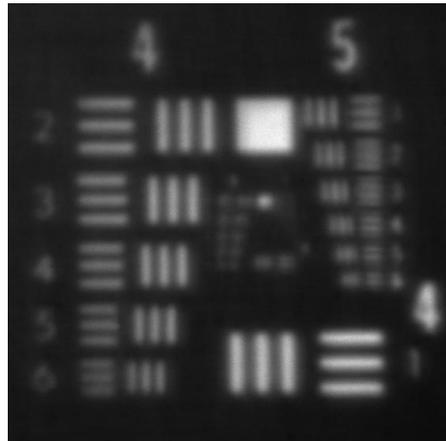
Z = -6 cm.

Z = -10 cm.

Single lens

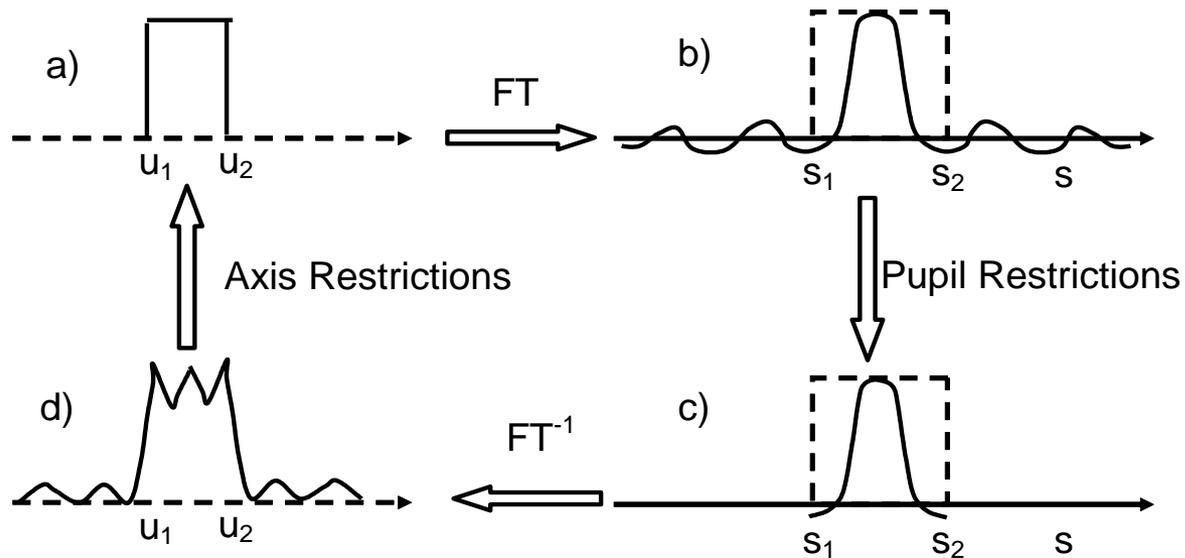


Multiplexed lens



Tailoring the axial response

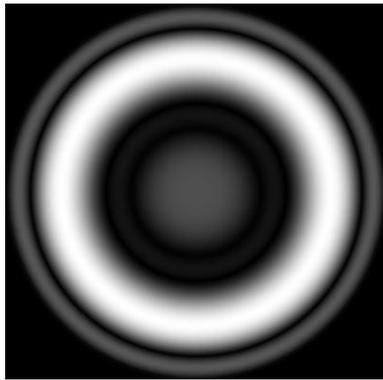
$$E(u) \propto \int_{-\infty}^{\infty} p(s) \exp(-i2\pi us) ds = P(u)$$



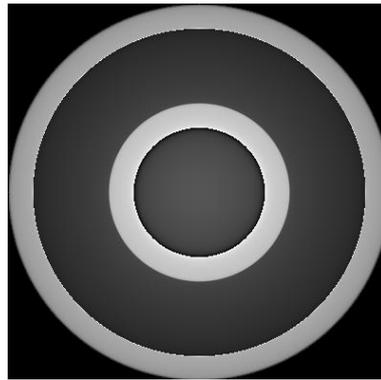
Tailoring the axial response

Encoding Complex pupils in Phase Only SLMs

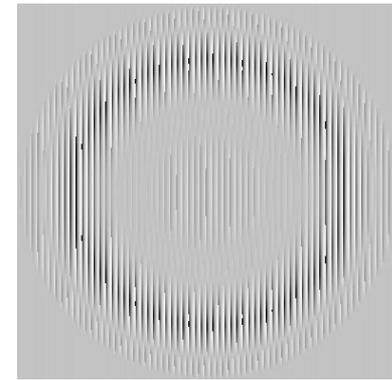
NARROW RECTANGLE



modulus

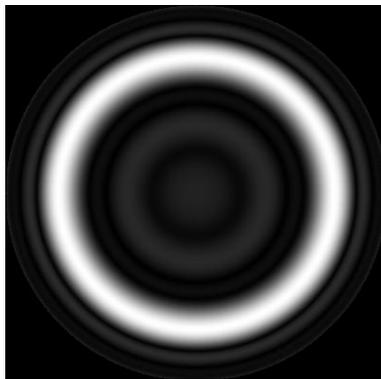


phase

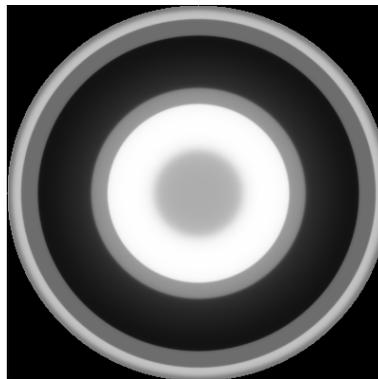


encoded pupil

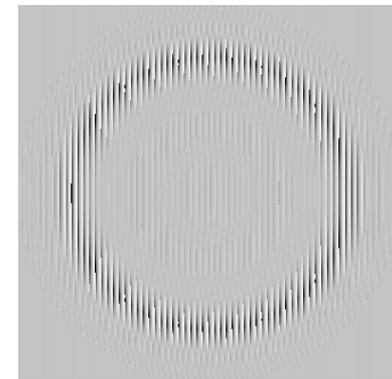
TRIANGLE



modulus

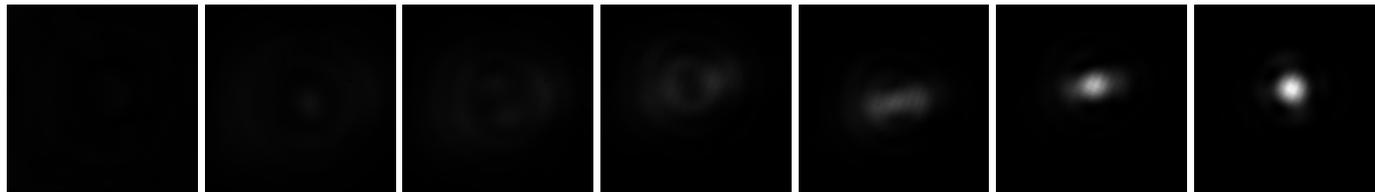


phase



encoded pupil

Tailoring the axial response



$Z = -12$

$Z = -10$

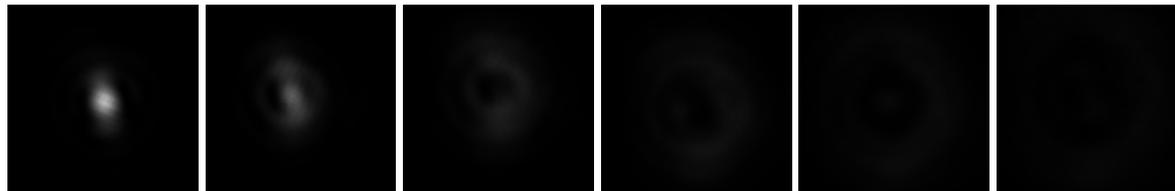
$Z = -8$

$Z = -6$

$Z = -4$

$Z = -2$

$Z = 0$



$Z = 2$

$Z = 4$

$Z = 6$

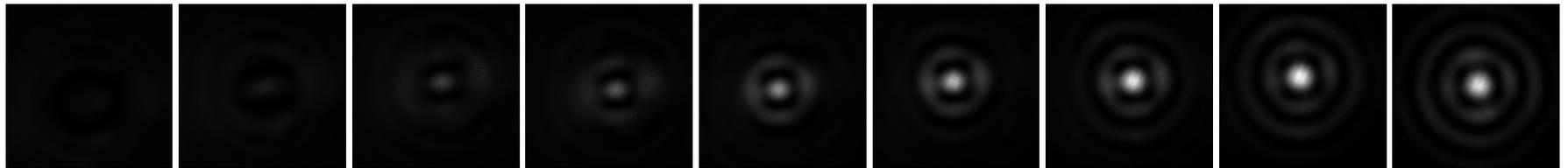
$Z = 8$

$Z = 10$

$Z = 12$

UNIFORM PUPIL

Tailoring the axial response



Z = -18

Z = -16

Z = -14

Z = -12

Z = -10

Z = -8

Z = -6

Z = -4

Z = -2



Z = 0

Z = 2

Z = 4

Z = 6

Z = 8

Z = 10

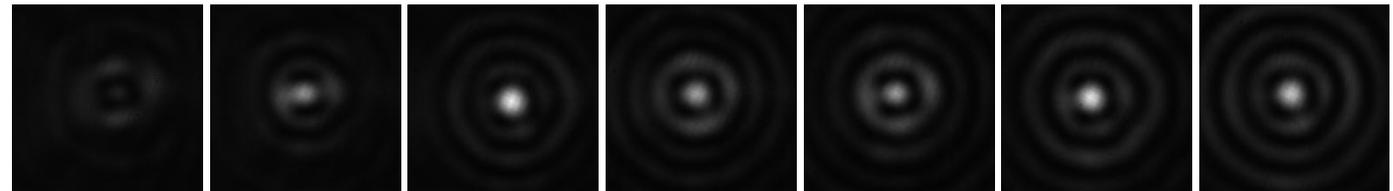
Z = 12

Z = 14

Z = 16

NARROW RECTANGLE

Tailoring the axial response



Z = -44

Z = -40

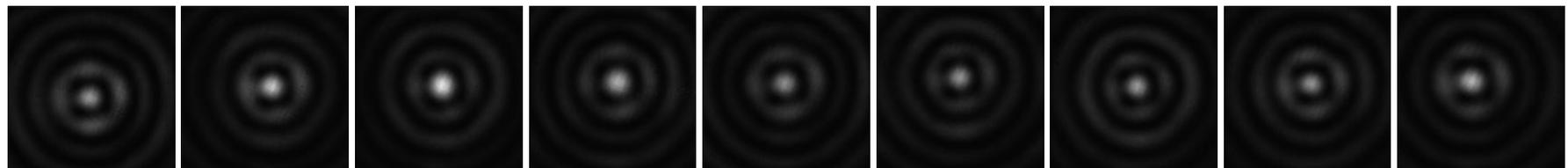
Z = -36

Z = -32

Z = -28

Z = -24

Z = -20



Z = -16

Z = -12

Z = -8

Z = -4

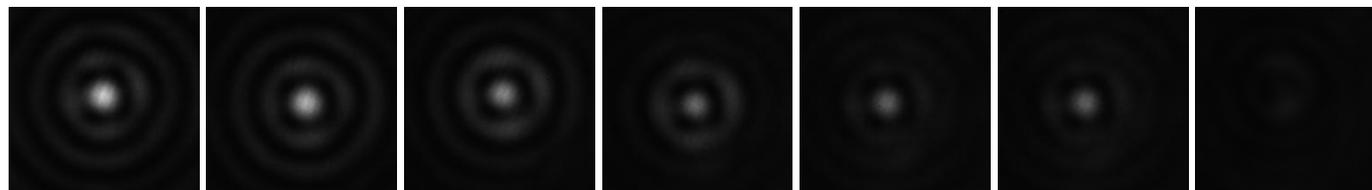
Z = 0

Z = 4

Z = 8

Z = 12

Z = 16



Z = 20

Z = 24

Z = 28

Z = 32

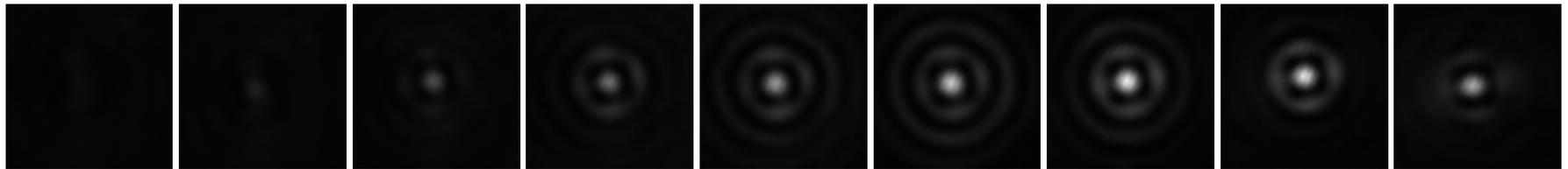
Z = 36

Z = 40

Z = 44

WIDE RECTANGLE

Tailoring the axial response



Z = -48

Z = -44

Z = -40

Z = -36

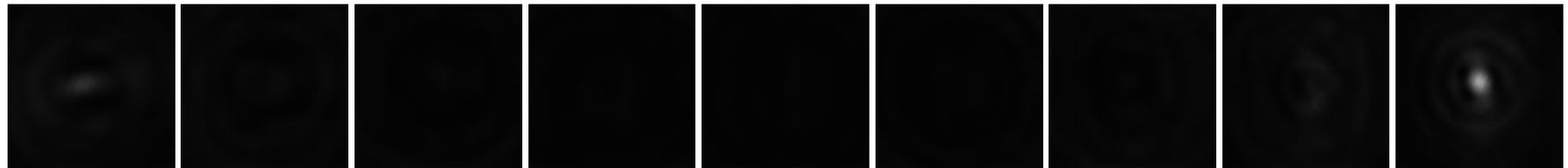
Z = -32

Z = -28

Z = -24

Z = -20

Z = -16



Z = -12

Z = -8

Z = -4

Z = 0

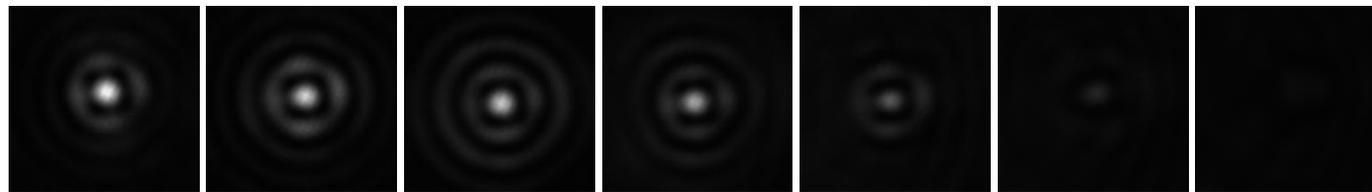
Z = 4

Z = 8

Z = 12

Z = 16

Z = 20



Z = 24

Z = 28

Z = 32

Z = 36

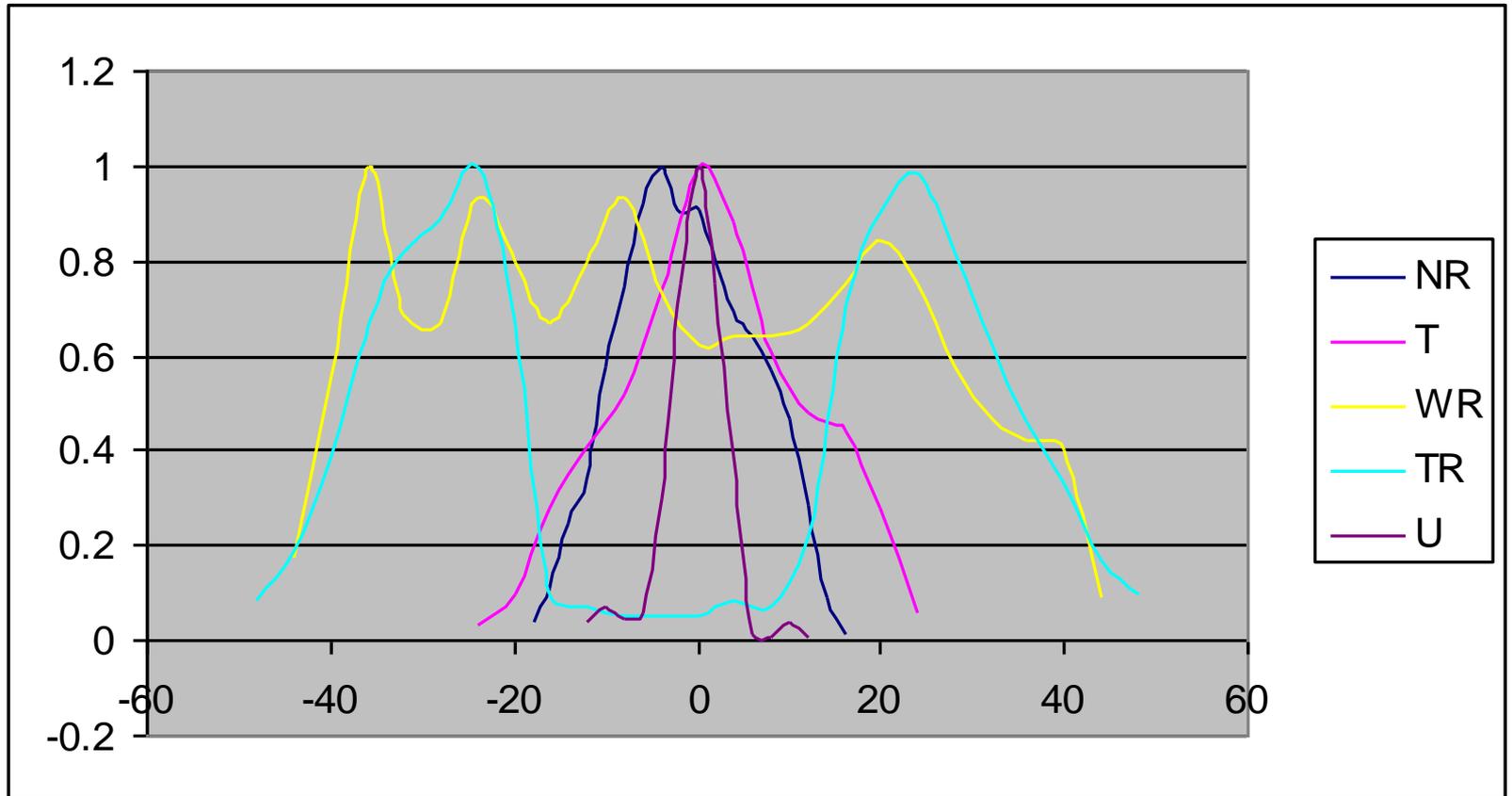
Z = 40

Z = 44

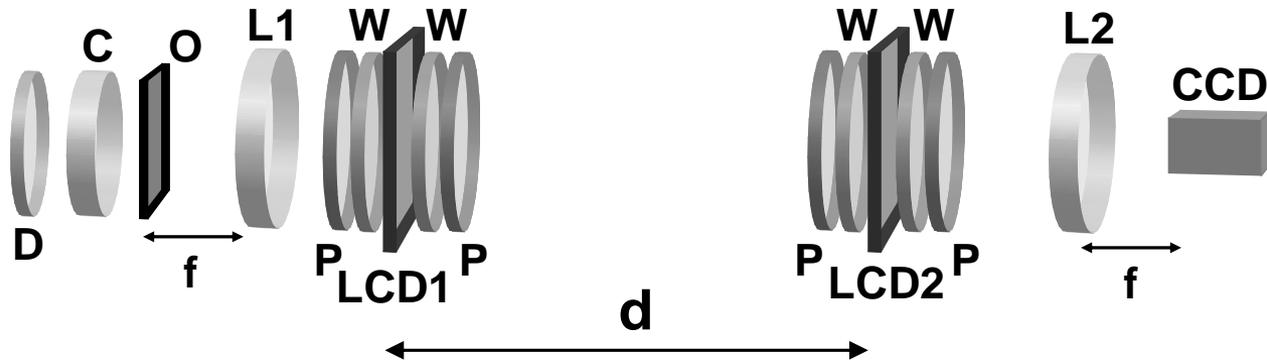
Z = 48

TWO RECTANGLES

Tailoring the axial response



Anamorphic Zoom



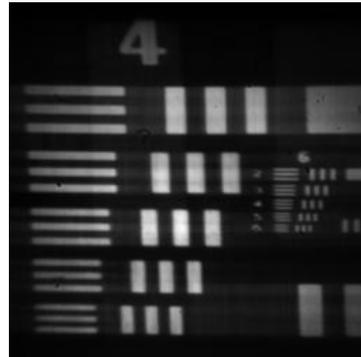
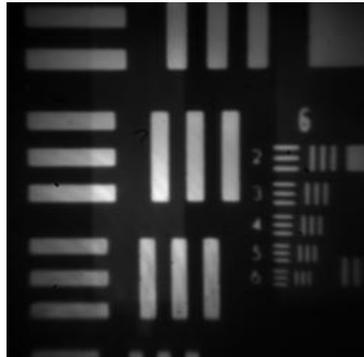
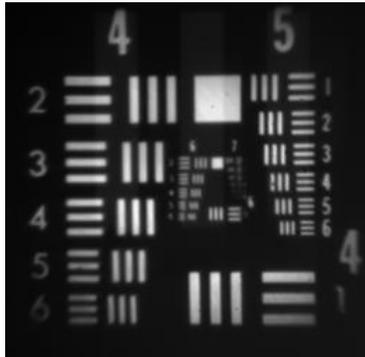
Without Zoom

Zoom ($x=y$)

Zoom (x)

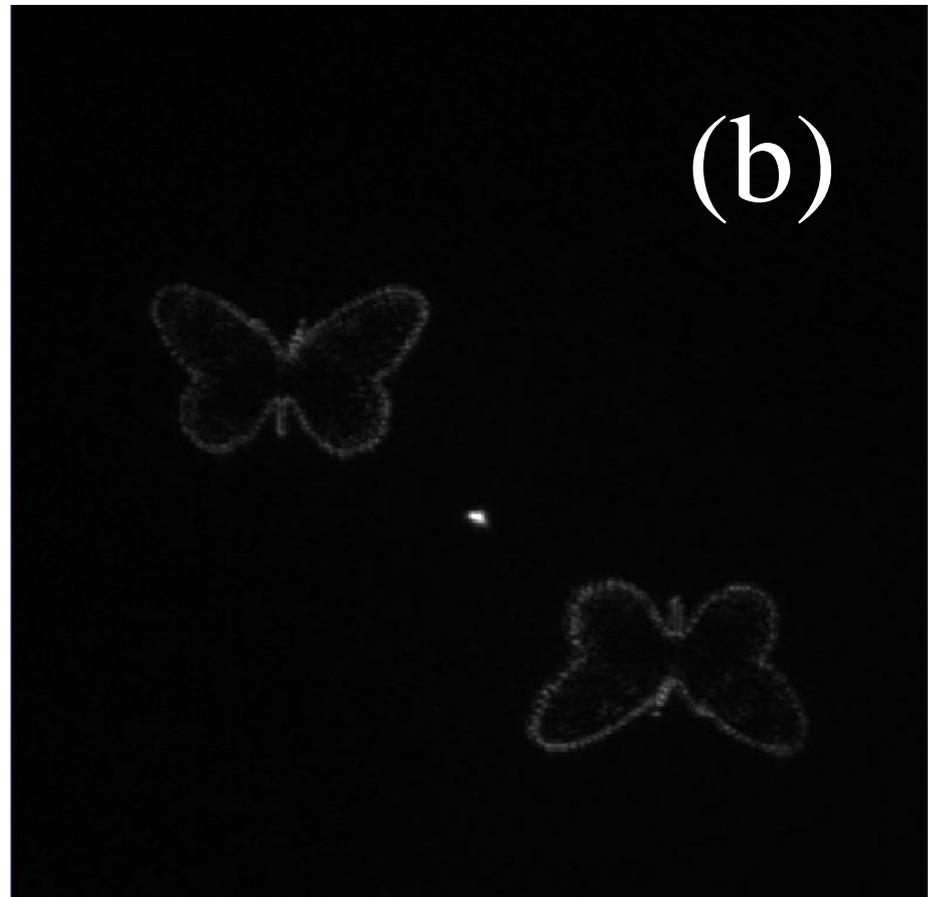
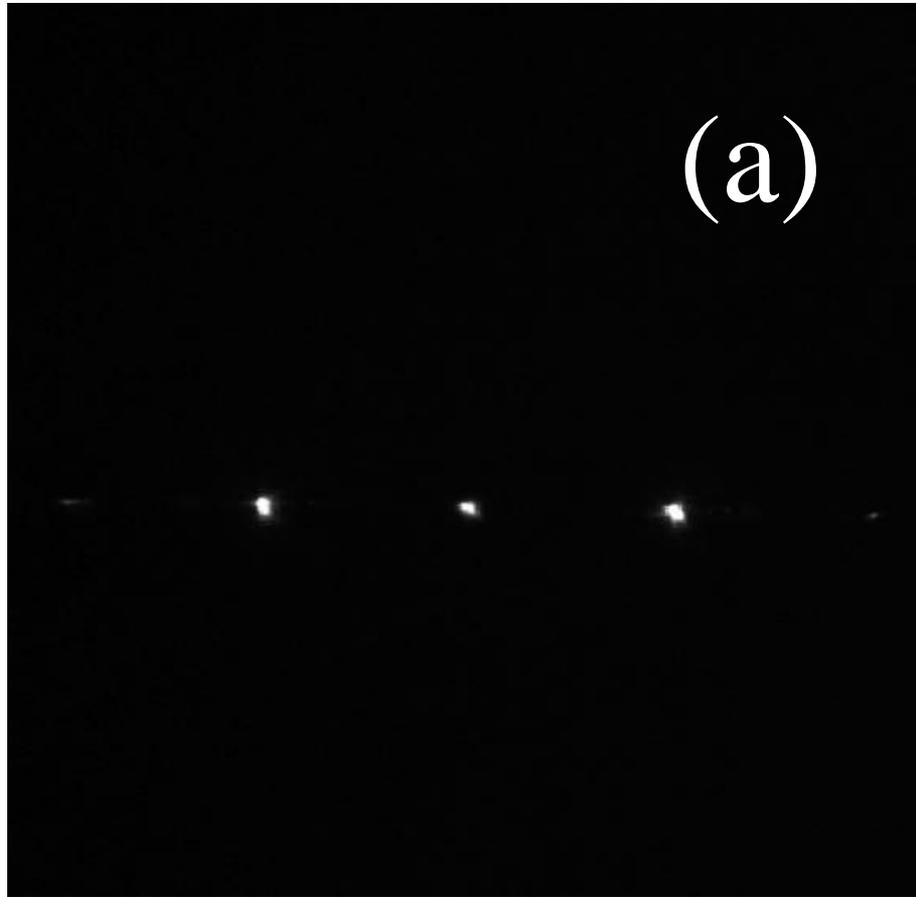
Zoom (y)

Anamorphic Rotated

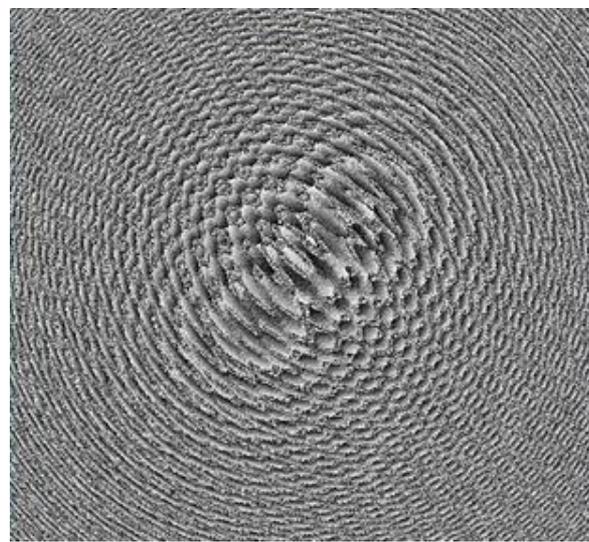
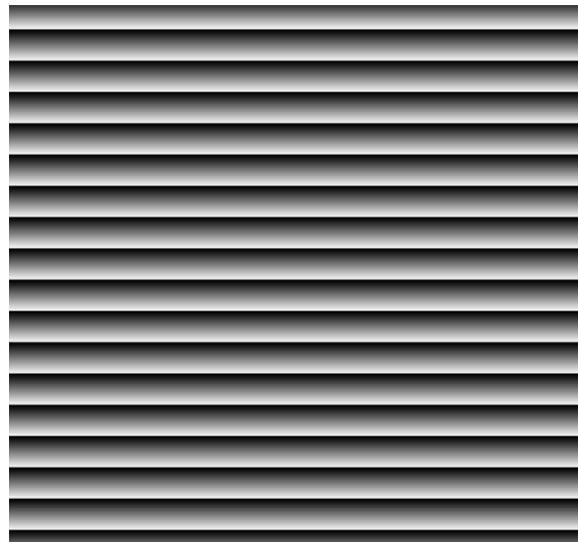
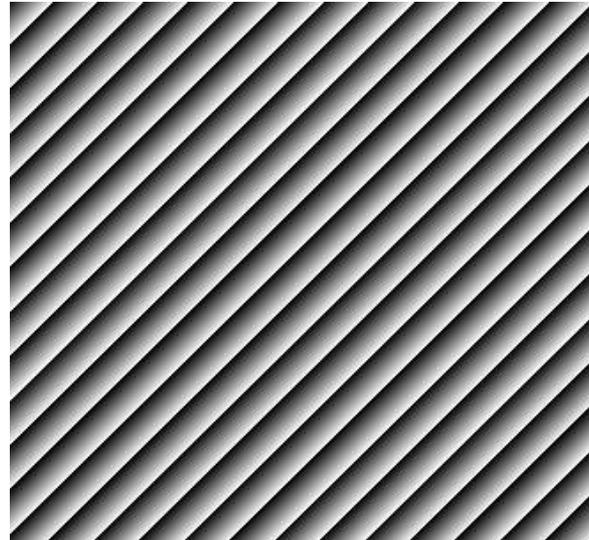
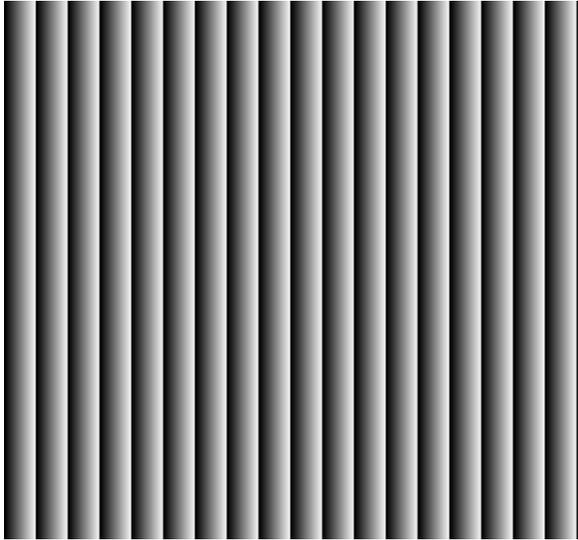


Phase fluctuation phenomenon

Effects on Diffractive Optics



3 multiplexed Blazed grating



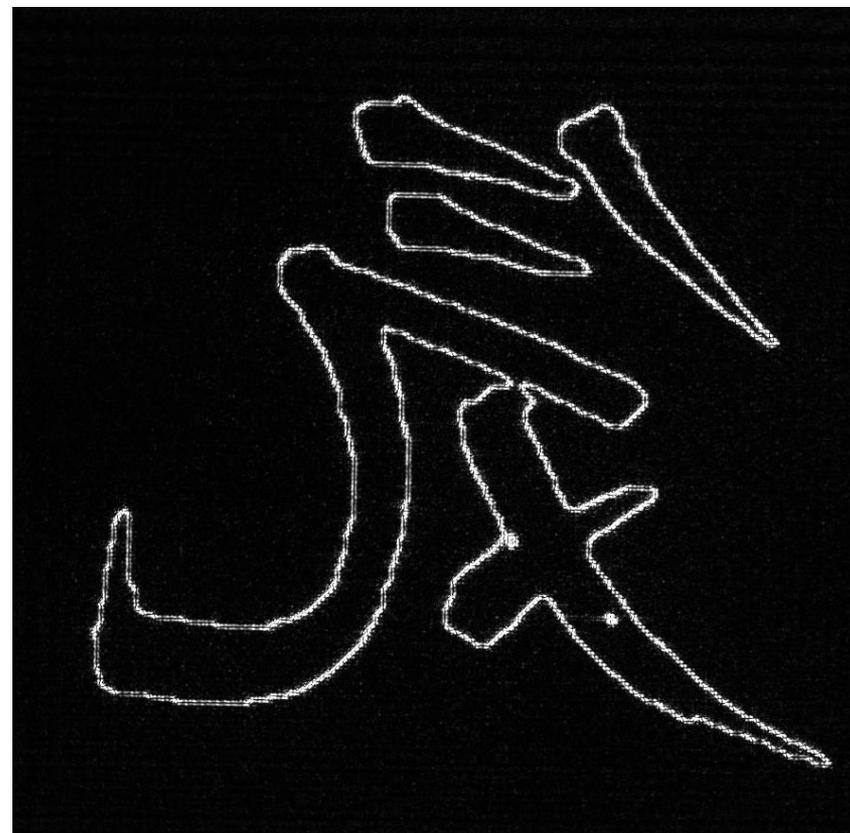
3 multiplexed Blazed grating

- **Period (18), angle (0,45,90), focal spherical lens (200)**

Random Multiplex



Phase hologram



Research team



J. Campos, J.C. Escalera, A. Lizana, O. López-Coronado, A. Peinado, M. J. Yzuel
Universitat Autònoma de Barcelona, SPAIN.



I. Moreno
Universidad Miguel Hernández, SPAIN.



Universitat d'Alacant
Universidad de Alicante

A. Márquez
Universidad de Alicante, SPAIN.



J. Nicolás
ALBA Synchrotron Light Source Facility, SPAIN.



C. Lemmi
Universidad de Buenos Aires, ARGENTINA.



SAN DIEGO STATE
UNIVERSITY

J. A. Davis
San Diego State University. San Diego. USA.

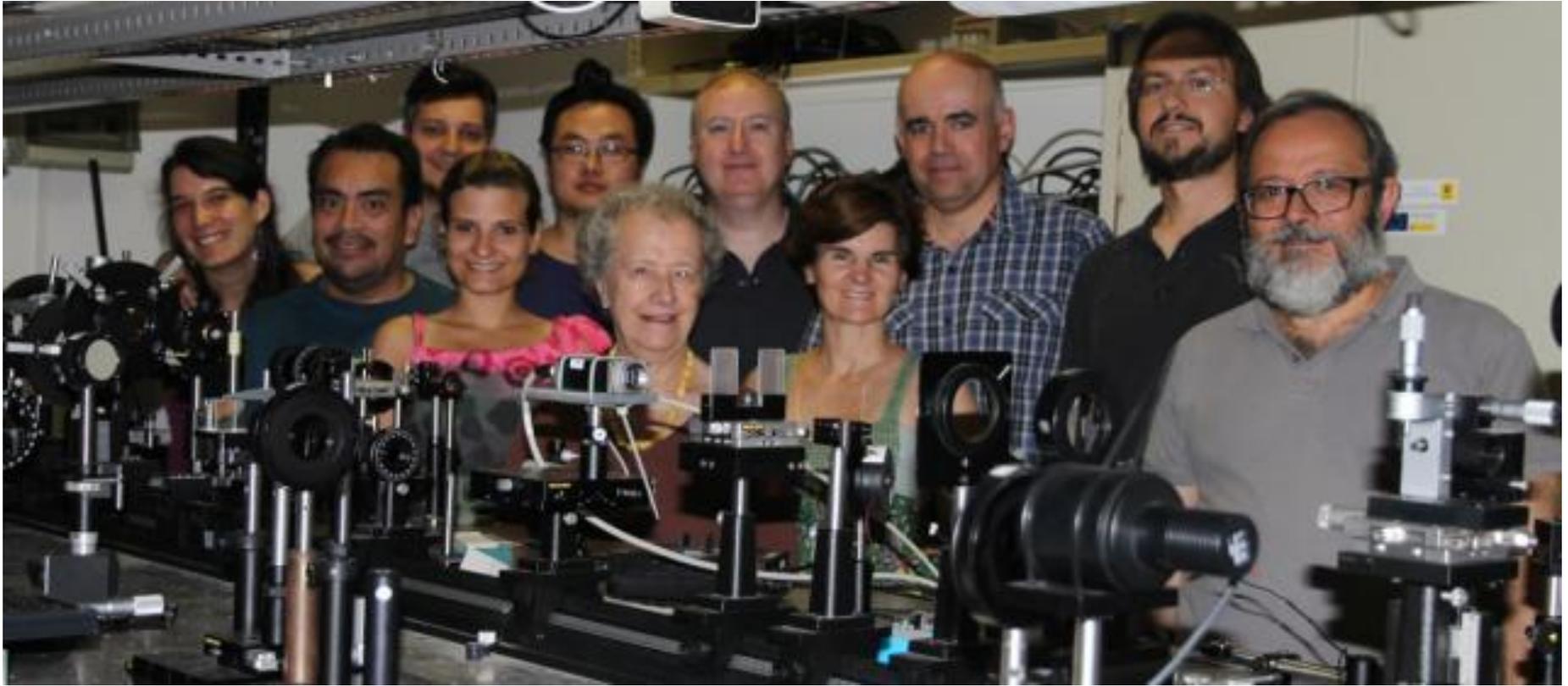
Universitat Autònoma de Barcelona



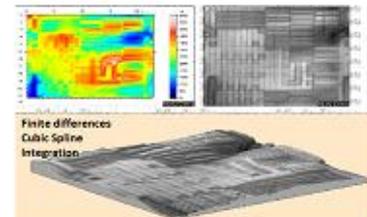
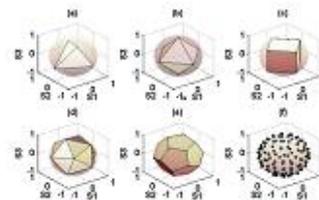
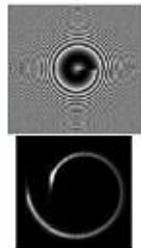
www.uab.cat

Universitat Autònoma de Barcelona



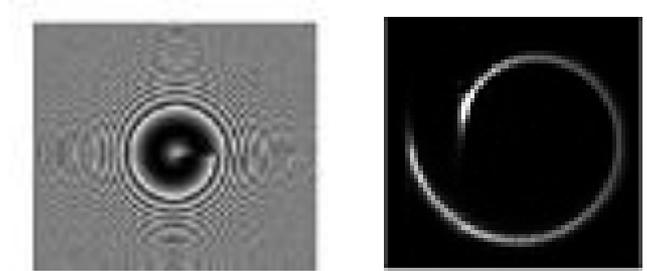


<http://grupsderecerca.uab.cat/mipoptilab/>

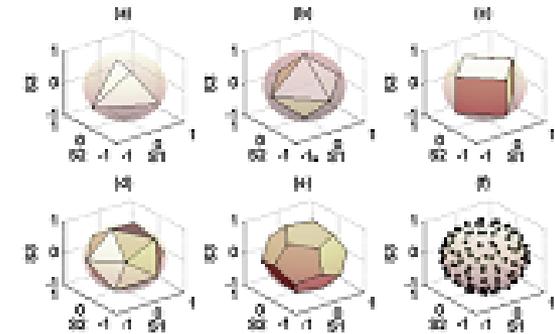




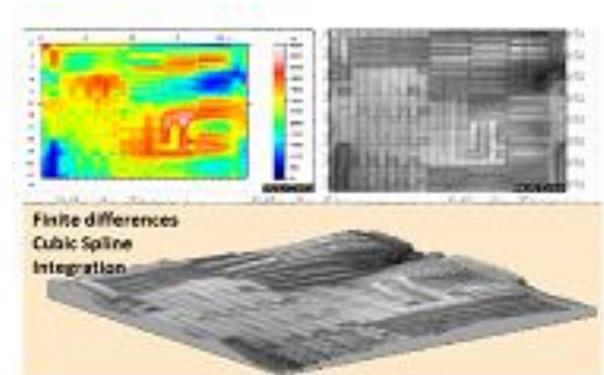
1) LCD characterization and Diffractive Optics



2) Polarization control, polarimeters and applications



3) Optical metrology



SPIE

The international Society
for Optics and Photonics

www.spie.org

SPIE at a Glance

264,000
Constituent



19,000
Members



166
Countries



20
Annual Conferences



650
Corporate Members



300
Student Chapters

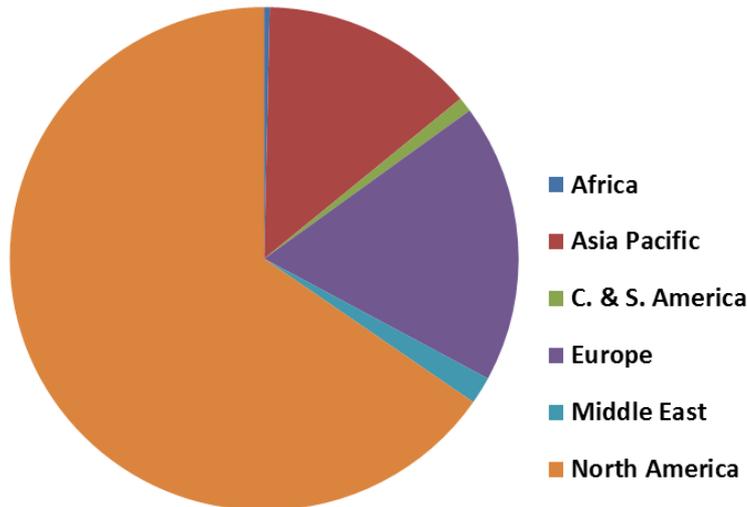


SPIE in Russia

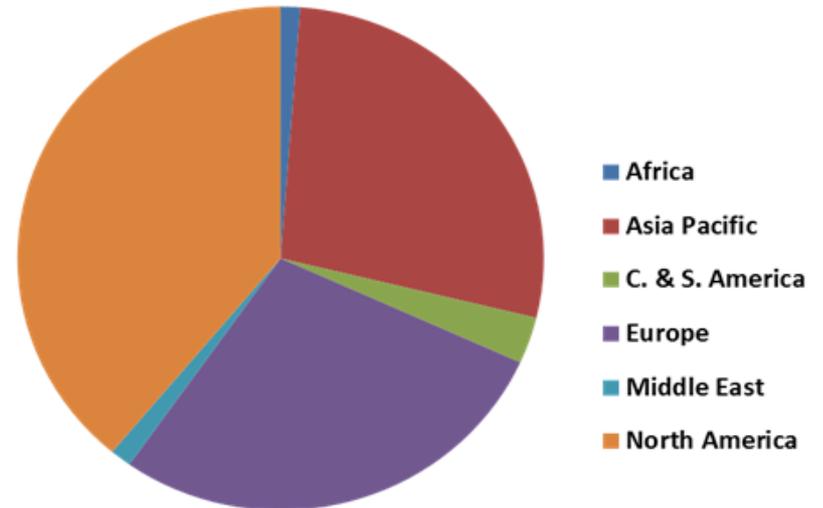
Russia:

14 Student Chapters
239 Student Members
80 Regular Members
6 Senior Members
5 Fellows
3 Corporate Members

18,500 Total Members
80 in Russia



7,500 Student Members
239 in Russia



SPIE Student Chapters in Russia

- Saint–Petersburg Acad Univ
Russian Acad of Science
- Kazan National Research Tech
Univ
- Bauman Moscow State Technical
Univ
- Lomonosov Moscow State Univ
Chapter
- ITMO University Chapter
- Saratov State Univ
- V.E. Zuev Institute of
Atmospheric Optics
- Vladivostok Student Chapter
- Samara Student Chapter
- Saint-Petersburg State Univ of
Aerospace
- Institute of Automation and
Electrometry
- Nizhny Novgorod Student
Chapter
- Povolzhskiy State Univ of
Telecommunications and
Informatics Chapter
- National Research Univ. of
Electronic Tech
National
Research Univ. of Electronic Tech

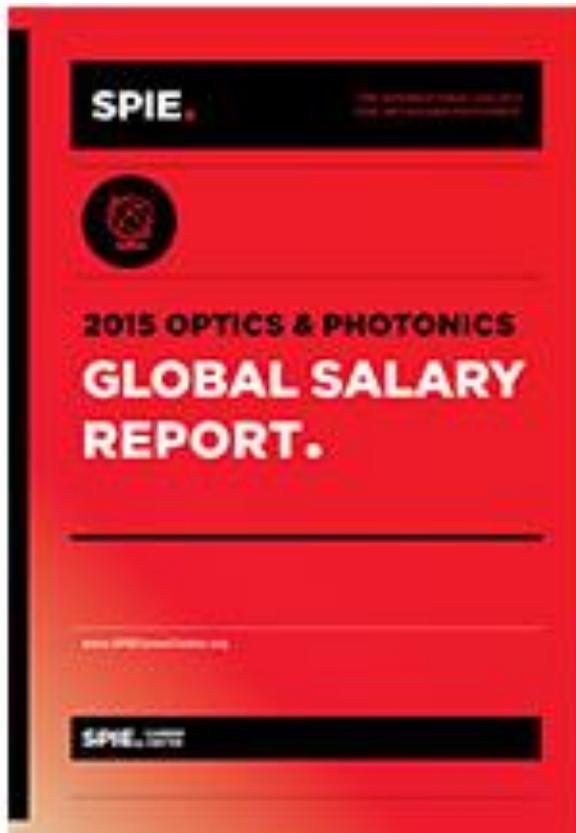
SPIE Student Chapter Map



SPIE Salary Survey



79% love their work and feel fortunate to get paid for doing it.

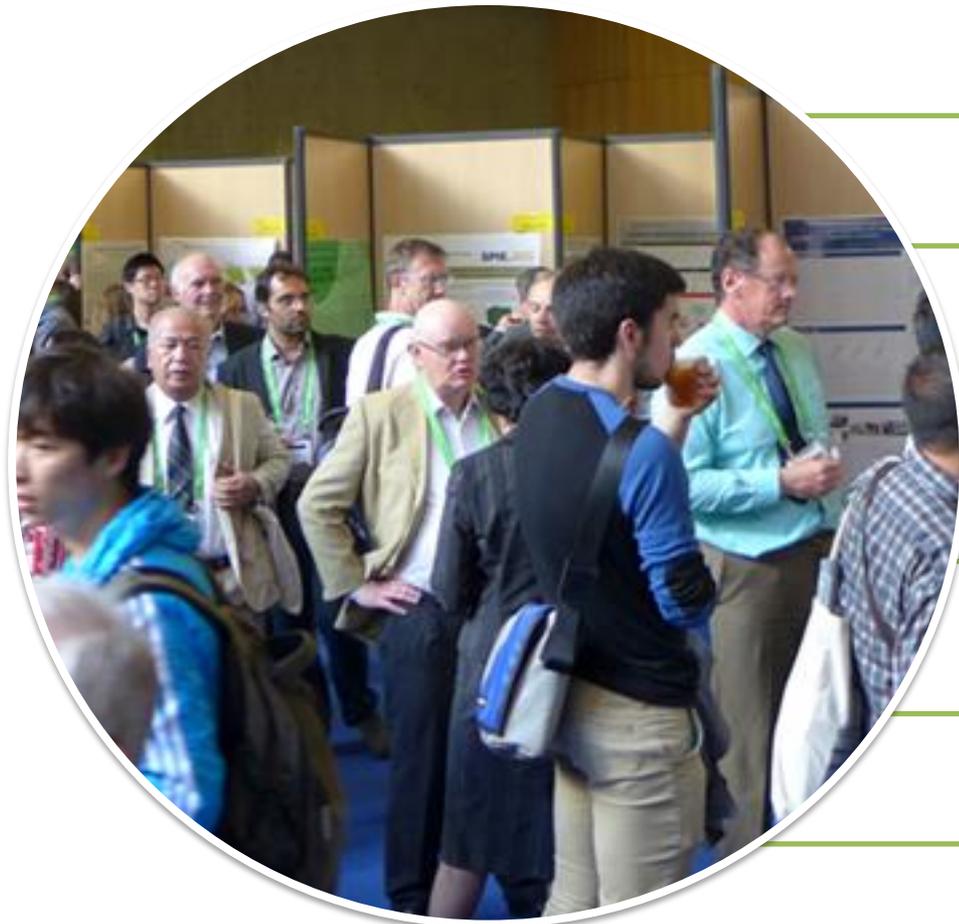


MEDIAN SALARY BY EMPLOYER TYPE



Major SPIE Conferences

Plus many smaller meetings



SPIE. REMOTE SENSING

SPIE. PHOTONICS WEST

SPIE. PHOTONICS EUROPE

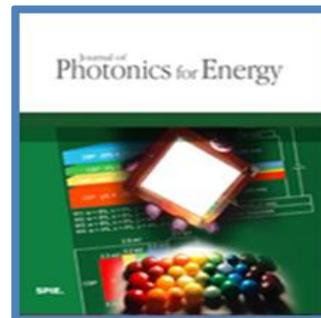
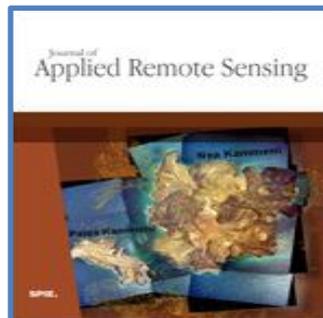
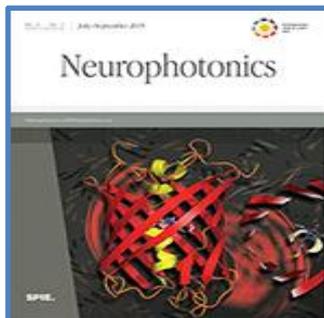
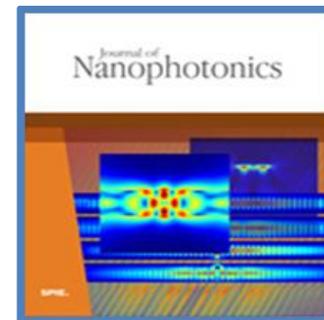
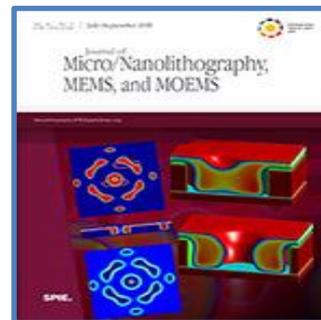
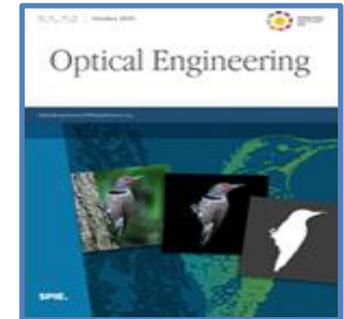
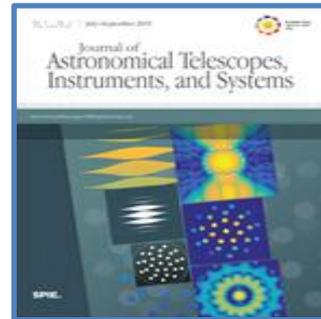
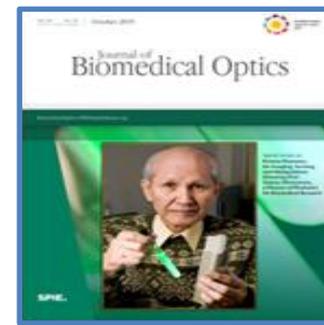
SPIE. OPTICS+ PHOTONICS

SPIE. SECURITY+ DEFENCE

SPIE. ASTRONOMICAL TELESCOPES + INSTRUMENTATION

SPIE Digital Library

10 peer-reviewed journals,
ebooks and 430,000 papers



SPIE Altruistic Activities



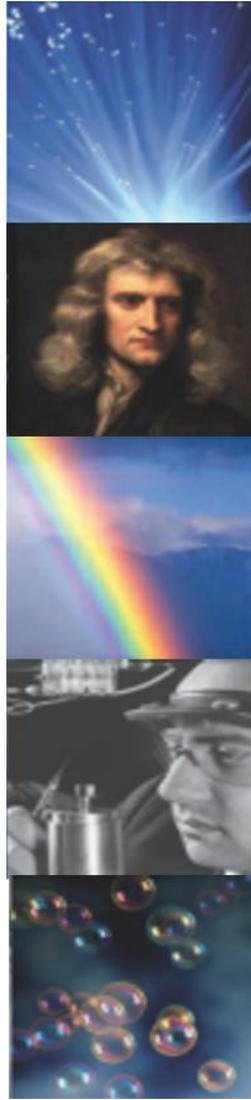
INTERNATIONAL
YEAR OF LIGHT
2015

Over \$5.2 million USD in support in 2015

- \$350,000 USD in Scholarships
- \$90,000 USD in Education Outreach Grants
- Educational outreach kits, posters and videos
- Summer schools, science fairs & best paper prizes
- Free SPIE Digital Library for developing nations
- UNESCO Active Learning in Optics and Photonics (ALOP) teacher training for developing nations
- Women in Optics events and planner
- International Year of Light Founding Partner

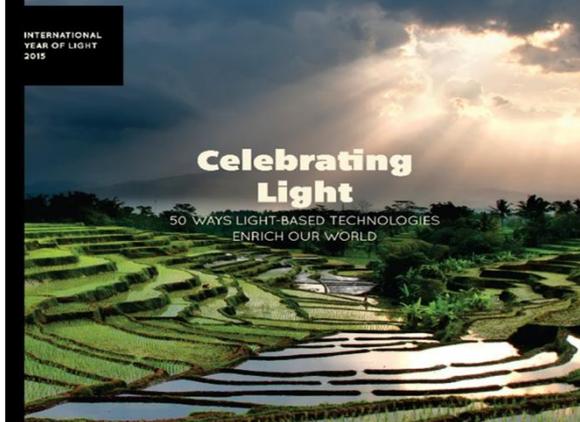
Your Membership Makes a Difference!

SPIE. the international society for optics and photonics





Light Painting World Alliance



25,000 SPIE IYL books distributed



IYL New Years in Australia



Story of Light Festival in India



UK IYL patron, Duke of York



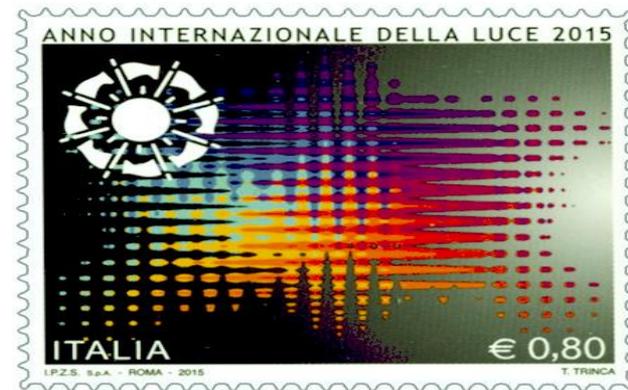
IYL song competition in Europe



IYL at CERN



Amsterdam rainbow train station



IYL stamps issued in 17 countries

Get Involved! www.spie.org



- Become an SPIE member
- Start a student chapter
- Apply for an outreach grant
- Educate the next generation
- Nominate a Fellow or Senior Member
- Present your research at a conference
- Become a reviewer
- Join a planning committee

ICO

International

Commission for Optics

www.e-ico.org

ICO

**Is organized in Territorial
Committees**

**Russian Federation
Committee**

ICO

**General Congress every 3 years
Next one in 21-25 August, 2017 in
Japan**

**The General Assembly meets every
3 years.**

ICO

Organizes Topical conferences

**Sponsor of meetings and
schools**

ICO Prizes and Awards

- ICO Prize

-ICO and IUPAP Optics Prize

ICOand ICTP Galieno Denardo Prize

-ICO Galileo Galilei Award

Thank you for
your attention